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## 13. ABSTRACT (Maximum 200 words)

The John A. Volpe National Transportation Systems Center (Volpe Center), in support of the Federal Aviation administration, Office of Environment and Energy, has developed Version 4.11 of the Integrated Noise Model (INM). The User's Guide for the Version 4.11 computer software is a supplement to INM, Version 3, User's Guide - Revision 1 for the Version 3.10 computer software released in June, 1992. The Version 4.11 supplement, prepared by the Volpe Center's Acoustics Facility, presents computer system requirements as well as installation procedures and enhancements. Specific enhancements discussed include: (1) the introduction of a takeoff profile generator; (2) the ability to account for terrain elevation around a specified airport; (3) the ability to compute the CNEL, WECNML, LEQDAY, and LEQNIGHT noise metrics; (4) the ability to account for airplane runup operations; (5) the ability to account for displaced runway thresholds during approach operations; (6) an enhancement to the noise contour computations; (7) an increase in the number of takeoff profile segments; and (8) enhancements to the echo file.

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# SI\* (MODERN METRIC) CONVERSION FACTORS

## APPROXIMATE CONVERSIONS TO SI UNITS

## APPROXIMATE CONVERSIONS FROM SI UNITS

Symbol	When You Know	Multiply By	To Find	Symbol	Symbol	When You Know	Multiply By	To Find	Symbol
<b>LENGTH</b>					<b>LENGTH</b>				
in	inches	25.4	millimeters	mm	mm	millimeters	0.039	inches	in
ft	feet	0.305	meters	m	m	meters	3.28	feet	ft
yd	yards	0.914	meters	m	m	meters	1.09	yards	yd
mi	miles	1.61	kilometers	km	km	kilometers	0.621	miles	mi
<b>AREA</b>					<b>AREA</b>				
in <sup>2</sup>	square inches	645.2	millimeters squared	mm <sup>2</sup>	mm <sup>2</sup>	millimeters squared	0.0016	square inches	in <sup>2</sup>
ft <sup>2</sup>	square feet	0.093	meters squared	m <sup>2</sup>	m <sup>2</sup>	meters squared	10.764	square feet	ft <sup>2</sup>
yd <sup>2</sup>	square yards	0.836	meters squared	m <sup>2</sup>	ha	hectares	1.195	square yards	ac
ac	acres	0.405	hectares	ha	km <sup>2</sup>	kilometers squared	2.47	acres	mi <sup>2</sup>
mi <sup>2</sup>	square miles	2.59	kilometers squared	km <sup>2</sup>			0.386	square miles	
<b>VOLUME</b>					<b>VOLUME</b>				
fl oz	fluid ounces	29.57	milliliters	ml	ml	milliliters	0.034	fluid ounces	fl oz
gal	gallons	3.785	liters	l	l	liters	0.264	gallons	gal
ft <sup>3</sup>	cubic feet	0.028	meters cubed	m <sup>3</sup>	m <sup>3</sup>	meters cubed	35.71	cubic feet	ft <sup>3</sup>
yd <sup>3</sup>	cubic yards	0.765	meters cubed	m <sup>3</sup>	m <sup>3</sup>	meters cubed	1.307	cubic yards	yd <sup>3</sup>
<b>MASS</b>					<b>MASS</b>				
oz	ounces	28.35	grams	g	g	grams	0.035	ounces	oz
lb	pounds	0.454	kilograms	kg	kg	kilograms	2.202	pounds	lb
T	short tons (2000 lb)	0.907	megagrams	Mg	Mg	megagrams	1.103	short tons (2000 lb)	T
<b>TEMPERATURE (exact)</b>					<b>TEMPERATURE (exact)</b>				
°F	Fahrenheit temperature	5(F-32)/9 or (F-32)/1.8	Celsius temperature	°C	°C	Celsius temperature	1.8C + 32	Fahrenheit temperature	°F
<b>ILLUMINATION</b>					<b>ILLUMINATION</b>				
fc	foot-candles	10.76	lux	lx	lx	lux	0.0929	foot-candles	fc
ft	foot-lamberts	3.426	candelas/m <sup>2</sup>	cd/m <sup>2</sup>	cd/m <sup>2</sup>	candelas/m <sup>2</sup>	0.2919	foot-lamberts	ft
<b>FORCE and PRESSURE or STRESS</b>					<b>FORCE and PRESSURE or STRESS</b>				
lbf	poundforce	4.45	newtons	N	N	newtons	0.225	poundforce	lbf
psi	poundforce per square inch	6.89	kilopascals	kPa	kPa	kilopascals	0.145	poundforce per square inch	psi

\* SI is the symbol for the International System of Units

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<b>ILLUMINATION</b>				
fc	foot-candles	10.76	lux	lx
fl	foot-lamberts	3.426	candelas/m <sup>2</sup>	cd/m <sup>2</sup>
<b>FORCE and PRESSURE or STRESS</b>				
lbf	poundforce	4.45	newtons	N
psf	poundforce per square inch	6.89	kilopascals	kPa

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mm <sup>2</sup>	millimeters squared	0.0016	square inches	in <sup>2</sup>
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m <sup>2</sup>	meters squared	1.195	square yards	yd <sup>2</sup>
ha	hectares	2.47	acres	ac
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<b>VOLUME</b>				
ml	milliliters	0.034	fluid ounces	fl oz
l	liters	0.264	gallons	gal
m <sup>3</sup>	meters cubed	35.71	cubic feet	ft <sup>3</sup>
m <sup>3</sup>	meters cubed	1.357	cubic yards	yd <sup>3</sup>
<b>MASS</b>				
g	grams	0.035	ounces	oz
kg	kilograms	2.202	pounds	lb
Mg	megagrams	1.103	short tons (2000 lb)	T
<b>TEMPERATURE (exact)</b>				
°C	Celsius temperature	1.8C + 32	Fahrenheit temperature	°F
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lx	lux	0.0929	foot-candles	fc
cd/m <sup>2</sup>	candelas/m <sup>2</sup>	0.2919	foot-lamberts	fl
<b>FORCE and PRESSURE or STRESS</b>				
N	newtons	0.225	poundforce	lbf
kPa	kilopascals	0.145	poundforce per square inch	psf

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## 1. INTRODUCTION

During June, 1992,, through December, 1993,, the John A. Volpe National Transportation Systems Center ((Volpe Center)), in support of the Federal Aviation Administration, Office of Environment and Energy, developed Version 4.11 of the Integrated Noise Model ((INM)). The User's Guide for the Version 4.11 computer software, prepared by the Volpe Center's Acoustics Facility, is a supplement to the Integrated Noise Model ((INM)), Version 3,, User's Guide - Revision 1<sup>1</sup> for the Version 3.10 computer software released in June, 1992.. Section 1.0 of the supplementary document presents computer system requirements and installation procedures for INM Version 4.11.. Section 2.0 describes the user's implementation of several new capabilities, including descriptive examples. Appendix A describes the technical revisions made to several internal algorithms - primarily revisions which are transparent to INM users. Appendices B and C,, respectively, present a technical discussion of two new capabilities, the takeoff profile generator and the capability to account for airplane **runup** operations. Appendix D presents a copy of the INM Input Testcase, revised to reflect INM Version 4.11 enhancements. Appendix E contains a copy of the User's Manual for the WINM computer software, an INM Version 4.11 plotting program for use with Microsoft Windows.

### 1.1 Computer System Requirements

INM Version 4.11 operates on an IBM Personal Computer (PC) -Compatible platform with the following minimum configuration:

- IBM PC-AT or compatible, Series 286 microprocessor;
- 3 MB of available hard disk space;
- 590 KB of Random Access Memory (RAM) or 3 MB of RAM, if operating the INM from a RAM disk, as discussed in Section 1.2.1 below;
- Math co-processor, Series 80287;; and
- Microsoft-compatible Disk Operating System ((MSDOS)) Version 3.3..

In addition, the CONFIG.SYS file on the PC slated for INM Version 4.11 installation must contain the following lines: **BUFFERS=30;** and **FILES=30..**

### 1.2 Installation

The files on the INM Version 4.11 system diskette have been stored in a compressed format using the PKZIP Version 1.1 utility software [Copyright ((c)) 1990 PKWare,, Inc.]. With the source drive prompt displayed on the screen, execute the UNPACK batch file to install INM Version 4.11 on your PC:

- UNPACK <SOURCE DRIVE> <TARGET DRIVE>

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This will assign the RAM drive, i.e., the D-drive, to operate within the subdirectory **C:\RAM** on the hard drive. Note: It is extremely important to remember that each time the PC is reset or its power is turned off, the information stored on the **RAM** drive will be lost. As a result, if the **INM** is run from the RAM drive, all files must be copied to a physical drive, e.g., a floppy drive, prior to powering-off the PC.

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## 2. IMPLEMENTATION OF INM VERSION 4.11 ENHANCEMENTS

This Section of the document describes the methodology for implementing INM Version 4.11 enhancements. It includes a background discussion of the enhancements, a brief discussion of the need for the enhancements, and example implementation of the enhancements. The following enhancements are discussed: (1) the takeoff profile generator; (2) the ability to account for terrain elevation around a specified airport; (3) the ability to compute the **CNEL**, **WECPNL**, **LEQDAY**, and **LEQNIGHT** noise metrics; (4) the ability to account for airplane **runup** operations; (5) the ability to account for runway thresholds during approach operations; (6) an enhancement to the noise contour computations; (7) an increase in the number of takeoff profile segments; and (8) enhancements to the echo file.

### 2.1 Takeoff Profile Generator

This enhancement allows for the computation of airplane takeoff profiles based on the user-supplied airport elevation and temperature entry in the SETUP section of the INM input file. The takeoff profiles are utilized by the INM in the computation of all noise metrics. Previous versions of the INM utilize takeoff profiles which were based on standard-day conditions, i.e., temperature of **59°F** and airport elevation of zero **ft** Above Mean Sea Level (**MSL**).. Previously, the **user**-supplied airport elevation (altitude) and temperature were only used to compute an atmospheric acoustic impedance correction.

The takeoff profile generator is made possible by the inclusion of standardized airplane operating procedures and performance coefficients in Data Base Number 11.. These procedures and coefficients are presented in References 2, 3, and 4, and accessible from the Data Base using the **ACDB11.EXE** computer program, supplied with the Version 4.11 release. With the exception of INM airplane numbers 1, 6, 7, 8, 10, 24, 56, 100, 101, and four of the new airplanes (INM airplane numbers 104 to 107) discussed further in Appendix A, the operating procedures and performance coefficients required for takeoff profile computation are included in Data Base Number 11.. For the airplanes without standard procedures and coefficients the takeoff profile for standard conditions is assumed regardless of the airport elevation and temperature. Note: The incorporation of the takeoff profile generator will not affect the standard approach profiles. The approach profiles are the same as employed in INM Version 3.10..

Operation of the profile generator is time-efficient and entirely transparent to the user. If other than standard-day conditions are specified by the user in the SETUP portion of the input file, the profile generator automatically computes the takeoff profiles using the airplane performance coefficients in Data Base Number 11 and the equations in the

Society of Automotive Engineers Aerospace Information Report 1845<sup>5</sup> ((SAE/AIR 1845)). When an airport elevation and temperature is not specified, the **INM** assumes standard conditions and utilizes the standard profiles included with Data Base Number **11**, i.e., the internal profile generator will not be exercised.

To insure the takeoff profiles and resultant noise metrics computed by **INM** Version 4 **..11** are reasonable for the **user**-defined input case, a runway length check has been instituted. When the computed ground roll segment of the takeoff profile exceeds the user-specified runway length, the user is notified of the discrepancy. A message similar to the following is included in the echo file.

●      **WARNING: COMPUTED GROUND ROLL ERROR FOR INM AIRPLANE 747200,,  
STAGE WEIGHT 7, -- EXCEEDS USER-DEFINED RUNWAY LENGTH  
BY X PERCENT FOR THE TAKEOFF ON TRACK TR1,RUNWAY 09L..**

In many cases this warning will indicate to the user that there is an error in the input file, possibly in the **user**-defined average yearly temperature, airport elevation, airport runway length, or airplane stage weight. In cases where the computed ground roll segment exceeds the runway length by more than **10** percent, the above message will be included in the echo file as a fatal error rather than a warning and the user will not be permitted to continue processing of the input case.

There may be instances where the user has correctly defined the input case and the computed ground roll segment exceeds the runway length by more than **10** percent. This apparent anomaly may be the result of using the average yearly temperature at the airport as an input. For example, a particular airport may be capable of operating a high **stage**-weight **B747** airplane in the early evening or during winter months only, when the temperature is significantly lower than the average yearly temperature. In such cases it is suggested that a user-defined profile be included in the input file.

In addition, there may be instances (e.g., high stage weights, high temperatures, and high airport elevations combined) where a negative rate-of-climb is computed. Consequently, a fatal error will occur and a profile will not be generated. In such instances, the user will be notified with a message similar to that below; it is suggested that a user-defined profile be included in the input file.

●      **FATAL: PROFILE FOR INM AIRPLANE 747200,, STAGE WEIGHT 7 CANNOT  
BE COMPUTED..**

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●      **FATAL: PROFILE FOR INM AIRPLANE 747200,, STAGE WEIGHT 7 CANNOT  
BE COMPUTED..**



longitude of a reference point at the airport (e.g., the beginning of the primary runway). In the following example the latitude and longitude are for the start of Runway **09L** at Boston-Logan.

- **ENTER 3 LETTER AIRPORT IDENTIFIER (EX. BOS):: BOS**
- **ENTER RUNWAY LAT COORD.. DEGS MINS SECS (EX. 42 21 20):: 42 21 20**
- **ENTER RUNWAY LON COORD.. DEGS MINS SECS (EX. 71 00 48):: 71 00 48**

The **MAKEFILE.EXE** program then computes the coordinates of the southeast corner of a one-degree by one-degree data-block based upon the start of the airport's primary runway being at the geographic center of the block. The computed southeast corner is displayed along with the four **RMC DEM** files required to construct the one-degree by one-degree data-block around the airport. The user is also given the option to overwrite an existing or create a new **BOS.3CD** file, where **BOS** is the three-letter airport identifier.

- **THE SE CORNER OF THE REQUIRED (1X1 DEG) DATA BLOCK IS: 41 52 70 31**
- **THE REQUIRED DEM FILES ARE:   NW FN=42071.3CD   NE FN=42070.3CD  
                                  SW FN=41071.3CD   SE FN=41070.3CD**
- **DO YOU WISH TO CREATE A NEW BOS.3CD FILE (Y/N)? Y**

The user should type **Y** to overwrite/create a new file. If the four **DEM** files exist in the current directory, the program will create the **BOS.3CD** file without further prompting. If **MAKEFILE.EXE** cannot find the required **DEM** files, it will request that the user enter the drive where the **DEM** files are resident. In addition, **MAKEFILE.EXE** will ask if the data are on the **RMC** CD-ROM and, if so, copy them into the current directory. If the four **DEM** files are not on the CD-ROM drive, **MAKEFILE.EXE** will request the path where the files can be found. The program will then construct the required **one-degree** by one-degree data-file, with the airport's primary runway at its approximate geographic center. The user will be informed that the file has been constructed, and the minimum and maximum elevation within the constructed one-degree by one-degree block will be provided.

- **WRITING OF BOS.3CD IS COMPLETE**

The example **BOS.3CD** file is now ready for implementation by the **INM**. To utilize the elevation data in the **BOS.3CD** file in the computation of source-to-receiver slant range, the user must specify, in the **SETUP** portion of the **INM** input file: (1)

the three-letter airport code which identifies the specific user **pre-processed** **..3CD** file; (2) the disk-drive location of the **..3CD** file (Note: It is not necessary to specify the location of the **..3CD** file if it is in the current directory; also, if the **..3CD** file resides in a subdirectory, the path to that subdirectory must be created prior to running **INM.**); and (3) the latitude and longitude of a user-defined reference point at the airport, where the X and Y coordinates of all defined runways must be referenced to this point. To insure that the user has identified the appropriate **..3CD** file, the **INPUT.EXE** program will test the user-defined reference point at the airport against the stored reference in the **..3CD** file.

In the following example the user has: (1) specified Boston's Logan International Airport; (2) identified the C-drive as the location for the **BOS.3CD** file; and (3) specified the latitude and longitude of a reference point at Boston-Logan.

● **SETUP::**

**TITLE <EXAMPLE IMPLEMENTATION OF ELEVATION ENHANCEMENT>**  
**AIRPORT <ELEVATION EXAMPLE>**

**CODE BOS**  
**DRIVE C**  
**LATITUDE 42 21 20**  
**LONGITUDE 71 00 48**

With the elevation enhancement invoked as described above, all noise-level computations are performed based upon the actual source-to-receiver slant range, rather than assuming a flat terrain as was the case in previous versions of the **INM.**

In addition, the data in the **BOS.3CD** file are used to compute the slope of a three-by-three arc-second tangential ground plane, with the receiver at its physical center. This ground plane is used in the computation of the source-to-receiver elevation-angle, beta, required by the lateral attenuation algorithm in the **INM.** The beta angle is defined as the angle subtended by the propagation path from the airplane to the receiver and the three-by-three arc-second ground plane. Figures 2-1 and 2-2,, respectively, depict the beta angle for two scenarios: (1) previous versions of the **INM** (i.e., flat terrain); and (2) **INM** Version 4.11..

### **2.3 CNEL,, WECPNL,, LEQDAY,, and LEQNIGHT Noise Metrics**

The capability to compute four additional noise metrics has been included in **INM** Version 4.11.. They are the Community Noise Equivalent Level ((**CNEL**)), Weighted Equivalent Continuous Perceived Noise Level ((**WECPNL**)), Equivalent Sound Level During Daytime Hours ((**LEQDAY**)), and Equivalent Sound Level During Nighttime Hours ((**LEQNIGHT**)). The addition of these four metrics brings the total number of metrics available for computation by the **INM** to eight ((**NEF**, **LEQ**, **LDN**, **TA**, **CNEL**, **WECPNL**, **LEQDAY**, and **LEQNIGHT**)). As was the case in previous

the three-letter airport code which identifies the specific user **pre-processed** **..3CD** file; (2) the disk-drive location of the **..3CD** file (Note: It is not necessary to specify the location of the **..3CD** file if it is in the current directory; also, if the **..3CD** file resides in a subdirectory, the path to that subdirectory must be created prior to running **INM.**); and (3) the latitude and longitude of a user-defined reference point at the airport, where the X and Y coordinates of all defined runways must be referenced to this point. To insure that the user has identified the appropriate **..3CD** file, the **INPUT.EXE** program will test the user-defined reference point at the airport against the stored reference in the **..3CD** file.

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● **SETUP::**

**TITLE <EXAMPLE IMPLEMENTATION OF ELEVATION ENHANCEMENT>**  
**AIRPORT <ELEVATION EXAMPLE>**

**CODE BOS**  
**DRIVE C**  
**LATITUDE 42 21 20**  
**LONGITUDE 71 00 48**

With the elevation enhancement invoked as described above, all noise-level computations are performed based upon the actual source-to-receiver slant range, rather than assuming a flat terrain as was the case in previous versions of the **INM.**

In addition, the data in the **BOS.3CD** file are used to compute the slope of a three-by-three arc-second tangential ground plane, with the receiver at its physical center. This ground plane is used in the computation of the source-to-receiver elevation-angle, beta, required by the lateral attenuation algorithm in the **INM.** The beta angle is defined as the angle subtended by the propagation path from the airplane to the receiver and the three-by-three arc-second ground plane. Figures 2-1 and 2-2,, respectively, depict the beta angle for two scenarios: (1) previous versions of the **INM** (i.e., flat terrain); and (2) **INM** Version 4.11..

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versions of the **INM**, Version **4.11** allows for the computation of all metrics simultaneously in grid mode or a single **user**-defined metric in contour mode for a given input case. A brief description of the **CNEL**, **WECPNL**, **LEQDAY**, and **LEQNIGHT** noise metrics follows:

- (1) Community Noise Equivalent Level ((CNEL)): The **CNEL** noise metric, which is primarily used in California, is similar to the Day-Night Sound Level (**LDN**) metric in that it incorporates the energy-averaged A-weighted sound level integrated over a **24-hour** period. However, unlike **LDN**, **CNEL** incorporates an additional penalty for operations occurring between the evening hours of **1900** and **2200** hours. For **CNEL**, a **3 dB** penalty is applied to operations occurring between **1900** and **2200** hours, and a **10 dB** penalty is applied to operations occurring between **2200** and **0700** hours. The equation for computing **CNEL** within the **INM** is as follows:

$$\text{CNEL} = \text{SEL} + 10 \log_{10} (N_{\text{day}} + 3N_{\text{eve}} + 10N_{\text{night}}) - 49.4,$$

where **SEL** = Sound Exposure Level in **dBA**;

$N_{\text{day}}$  = number of operations between **0700** and **1900** hours local time;

$N_{\text{eve}}$  = number of operations between **1900** and **2200** hours local time;

$N_{\text{night}}$  = number of operations between **2200** and **0700** hours local time;

and **49.4** = constant which normalizes **CNEL** to a **24-hour** period, (i.e.,  $10 \log_{10} (1/86,400 \text{ sec/day}) = -49.4$ ).

- (2) Weighted Equivalent Continuous Perceived Noise Level ((WECPNL)): The **WECPNL** noise metric, which is primarily used by the European Community, is based upon the **PNLT** noise metric and is computed within the **INM** as follows:

$$\text{WECPNL} = \text{EPNL} + 10 \log_{10} (N_{\text{day}} + 3N_{\text{eve}} + 10N_{\text{night}}) - 39.4,$$

where all definitions are the same as in **CNEL**, above, except:

**EPNL** = Effective **Perceived Noise** Level in **dB**; and

**39.4** =  $(49.4 - 10)$ ; where **49.4** is the constant which normalizes **WECPNL** to a **24-hour** period,

(i.e.,  $10 \log_{10}((1/86,400 \text{ secs/day})) = -49.4$ ); and -10 is the duration normalizing factor in the definition of **EPNL**.<sup>6</sup>

- (3) Equivalent Sound Level During Daytime Hours (LEODAY):  
The **LEODAY** noise metric is an energy summation of the aggregate environment, as measured in A-weighted decibel units (**dBA**) normalized to the **15-hour** time period from **0700** to **2200**. The equation for computing **LEODAY** within the **INM** is as follows:

$$\text{LEODAY} = \text{SEL} + 10 \log_{10}(\text{N}_{\text{day}} + \text{N}_{\text{eve}}) - 47.3,$$

where all definitions are the same as in **CNEL**, above, except:

$$47.3 = \text{constant which normalizes } \text{LEODAY} \text{ to the } 15\text{-hour period from } 0700 \text{ to } 2200, \text{ (i.e., } 10 \log_{10}((1/54,000 \text{ sec})) = -47.3).$$

- (4) Equivalent Sound Level During Nighttime Hours (LEONIGHT):  
The **LEONIGHT** noise metric is an energy summation of the aggregate environment, as measured in A-weighted decibel units (**dBA**) normalized to the **9-hour** time period from **2200** to **0700**. The equation for computing **LEONIGHT** within the **INM** is as follows:

$$\text{LEONIGHT} = \text{SEL} + 10 \log_{10}(\text{N}_{\text{night}}) - 45.1,$$

where all definitions are the same as in **CNEL**, above, except:

$$45.1 = \text{constant which normalizes } \text{LEONIGHT} \text{ to the } 9\text{-hour period from } 2200 \text{ to } 0700, \text{ (i.e., } 10 \log_{10}((1/32,400 \text{ sec})) = -45.1).$$

## 2.4 Airplane Runup Operations

This enhancement allows **INM** Version **4.11** to compute noise levels due to airplane engine **runup** operations. The need for this particular enhancement is recognized primarily around airplane maintenance facilities. To invoke this capability the user must define an airplane **runup** in the **TAKEOFF** section of the input file as follows:

```

• INT.INM.
  TAKEOFFS BY FREQUENCY:

  TRACK RUI RWY 09L STRAIGHT 50
    OPERATION 747200 RUNUP 1 D=30
    OPERATION 747200 STAGE 4 D=80
    <OR>
    OPERATION 747200 STAGE 4 D=80 RUNUP 1 D=30

```

(i.e.,  $10 \log_{10}((1/86,400 \text{ secs/day})) = -49.4$ ); and -10 is the duration normalizing factor in the definition of **EPNL**.<sup>6</sup>

- (3) Equivalent Sound Level During Daytime Hours (LEODAY):  
The **LEODAY** noise metric is an energy summation of the aggregate environment, as measured in A-weighted decibel units (**dBA**) normalized to the **15-hour** time period from **0700** to **2200**. The equation for computing **LEODAY** within the **INM** is as follows:

$$\text{LEODAY} = \text{SEL} + 10 \log_{10}(\text{N}_{\text{day}} + \text{N}_{\text{eve}}) - 47.3,$$

where all definitions are the same as in **CNEL**, above, except:

$$47.3 = \text{constant which normalizes } \text{LEODAY} \text{ to the } 15\text{-hour period from } 0700 \text{ to } 2200, \text{ (i.e., } 10 \log_{10}((1/54,000 \text{ sec})) = -47.3).$$

- (4) Equivalent Sound Level During Nighttime Hours (LEONIGHT):  
The **LEONIGHT** noise metric is an energy summation of the aggregate environment, as measured in A-weighted decibel units (**dBA**) normalized to the **9-hour** time period from **2200** to **0700**. The equation for computing **LEONIGHT** within the **INM** is as follows:

$$\text{LEONIGHT} = \text{SEL} + 10 \log_{10}(\text{N}_{\text{night}}) - 45.1,$$

where all definitions are the same as in **CNEL**, above, except:

$$45.1 = \text{constant which normalizes } \text{LEONIGHT} \text{ to the } 9\text{-hour period from } 2200 \text{ to } 0700, \text{ (i.e., } 10 \log_{10}((1/32,400 \text{ sec})) = -45.1).$$

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```

• INT.INM.
  TAKEOFFS BY FREQUENCY:

  TRACK RUI RWY 09L STRAIGHT 50
    OPERATION 747200 RUNUP 1 D=30
    OPERATION 747200 STAGE 4 D=80
    <OR>
    OPERATION 747200 STAGE 4 D=80 RUNUP 1 D=30

```

In addition, the specific location, e.g., the start of a runway or at a maintenance facility, and heading of the **runup** operation in the above user-defined example must be specified in the RUNWAYS section of the input file as discussed earlier in this section. A technical discussion of the airplane engine **runup** capability is presented in Appendix C.

## 2.5 Approach Runway Thresholds

The capability to account for displaced runway thresholds for approach operations has been added to **INM** Version 4.11. In previous versions of the **INM**, the runway touch-down point was assumed to be a fixed **954 ft** from the edge of the runway for airplanes with a three degree approach glide slope, and **572 ft** for the four airplanes with a five degree approach glide slope ((**INM** airplane numbers **74** to **77**)). With **INM** Version 4.11, a user-defined displaced threshold (**DT**), either positive or negative, is added to the fixed runway touch-down point. To insure realistic **DT's** are defined by the user, they are checked versus the runway coordinates. If discrepancies exist, the user is notified in the echo file, as appropriate. In the following example, a **1454 ft** runway touch-down point has been defined in the SETUP section of the input file for Runway **09L** (i.e., **500 ft** for the user-defined **DT** plus **954 ft** for the fixed touch-down point); and a runway touch-down point of **954 ft** has been defined for Runway **27R**:

```

●  SETUP::

    TITLE <EXAMPLE IMPLEMENTATION OF APPROACH RUNWAY THRESHOLD>
    AIRPORT <RUNWAY THRESHOLD EXAMPLE>

    ALTITUDE 23
    TEMPERATURE 12.66 C

    RUNWAYS
      RW 09L-27R  0 0 DT 500 TO 9487 -497 DT 0
                  <OR>
      RW 09L-27R  0 0 DT 500 TO 9487 -497
  
```

The above runway definition is depicted graphically below:

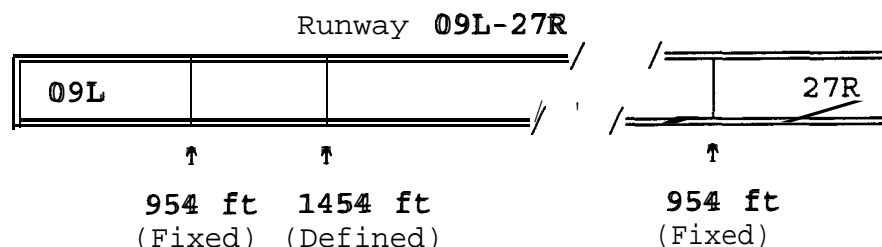


FIGURE 2-3:: RUNWAY DEFINITION

In addition, the specific location, e.g., the start of a runway or at a maintenance facility, and heading of the **runup** operation in the above user-defined example must be specified in the RUNWAYS section of the input file as discussed earlier in this section. A technical discussion of the airplane engine **runup** capability is presented in Appendix C.

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```

●   SETUP::

    TITLE <EXAMPLE IMPLEMENTATION OF APPROACH RUNWAY THRESHOLD>
    AIRPORT <RUNWAY THRESHOLD EXAMPLE>

    ALTITUDE 23
    TEMPERATURE 12.66 C

    RUNWAYS
      RW 09L-27R  0 0 DT 500 TO 9487 -497 DT 0
                  <OR>
      RW 09L-27R  0 0 DT 500 TO 9487 -497
  
```

The above runway definition is depicted graphically below:

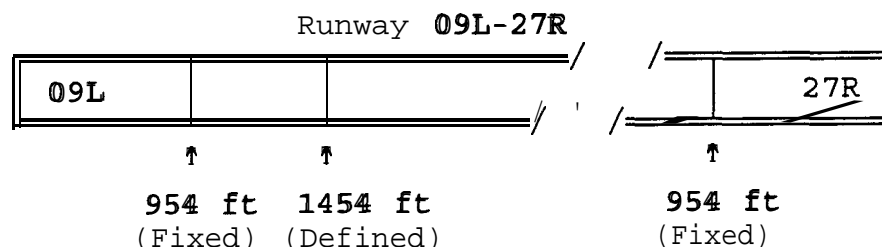


FIGURE 2-3:: RUNWAY DEFINITION





### 3. REFERENCES

- <sup>1</sup> Flythe, M.C., Integrated Noise Model Version 3, User's Guide - Revision 1, Report No. DOT/FAA/EE-92/02, Arlington, VA: CACTI, Inc. - Federal, June 1992..
- <sup>2</sup> Bishop, D.E., Mills, J.F., Update of Aircraft Profile Data for the Integrated Noise Model Computer Program, Volume 1, Report No. FAA-EE-91-02, Canoga Park, CA: Acoustical Analysis Associates, Inc., March 1992..
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- <sup>5</sup> Procedure for the Calculation of Airplane Noise in the Vicinity of Airports, SAE/AIR 1845, Warrendale, PA: Society of Automotive Engineers Committee A-21, Aircraft Noise, 1986..
- <sup>6</sup> Federal Aviation Regulations, Part 36, Noise Standards: Aircraft Type and Airworthiness Certification, Washington, D.C.: Federal Aviation Administration, December 1988..

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## APPENDIX A

### REVISIONS TO INM ALGORITHMS

This Appendix discusses, in general terms, revisions to several algorithms and subroutines included in **INM** Version 4.11.. It also discusses the rationale for these revisions and presents their effects on the noise contours, where applicable. The associated computer source code is not included. All revisions discussed below are transparent to the user in that they do not affect **user-operation** of the **INM**. However, these revisions will result in more accurate **INM** noise predictions and an increase in **INM** computational efficiency. They include: (1) revisions to the flight significance testing within the **INM**; (2) implementation of a **directivity** smoothing equation; (3) revisions to the dipole **directivity** pattern within the **INM**; and (4) revisions to the **INM** Data Base.

#### A.1 Flight Significance Testing.

The methodology employed for determining flight noise significance during grid computations has been streamlined in **INM** Version 4.11.. Rather than looping through each of the first four refinement levels individually and constructing the noise grid on a **level-by-level** basis, **INM** Version 4.11 begins by constructing the **17-by-17** point regular grid previously associated with the fourth refinement level, and setting all parameters associated with the **289** total points, including the noise significance flags for each point.

In restructuring the flight significance methodology, it was discovered that **INM** Version 3.10 was performing unnecessary (i.e., insignificant) noise computations due to improper setting of the flight significance flags. This impropriety had no effect on the computed noise levels but it did increase run-time unnecessarily. Revising the methodology for grid development, including the proper setting of flight significance flags, improved computation time by an estimated **40** percent over **INM** Version 3.10,, for comparable input cases.

#### A.2 Directivity Smoothing Equation

The **directivity** algorithm of **SAE/AIR1845** implemented for receivers behind start-of-takeoff roll, which is based on field-measured data published in 1980,, has been maintained within **INM** Version 4.11.. However, a **directivity** smoothing equation, operating as a function of distance, has been implemented. In previous versions of the **INM**, the **directivity** algorithm is applied to noise levels behind start-of-takeoff-roll regardless of lateral distance. In the 1980 study, measurements were made at distances from ~~start-of-takeoff-roll~~ of only **970** to **1280** ft. Recent studies<sup>67</sup> have indicated that **INM** Version 3.10 tends to underpredict noise levels behind ~~start-of-takeoff-roll~~ at distances of **3000** to **5000** ft., well beyond those represented in the 1980 study. This underprediction was especially evident for measurements made directly behind the airplane where

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The effect of the modified **directivity** pattern on the noise contours is depicted in Figures **A-3** and **A-4**, below. Figure **A-3** shows the effect on the **SEL** footprint for a single takeoff operation of the **B737-200** airplane (**INM** number **47**).. Figure **A-4** shows the effect on the **LDN** contour for the **INM** Input **Testcase** provided with **INM** Version **3.10**..

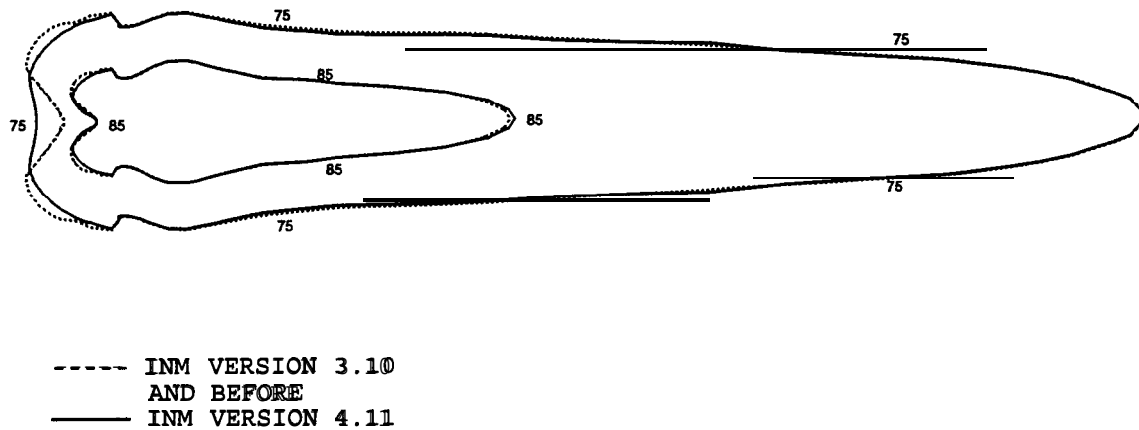


FIGURE **A-3**:: **SEL** TAKEOFF FOOTPRINT COMPARISON FOR **B737-200** AIRPLANE

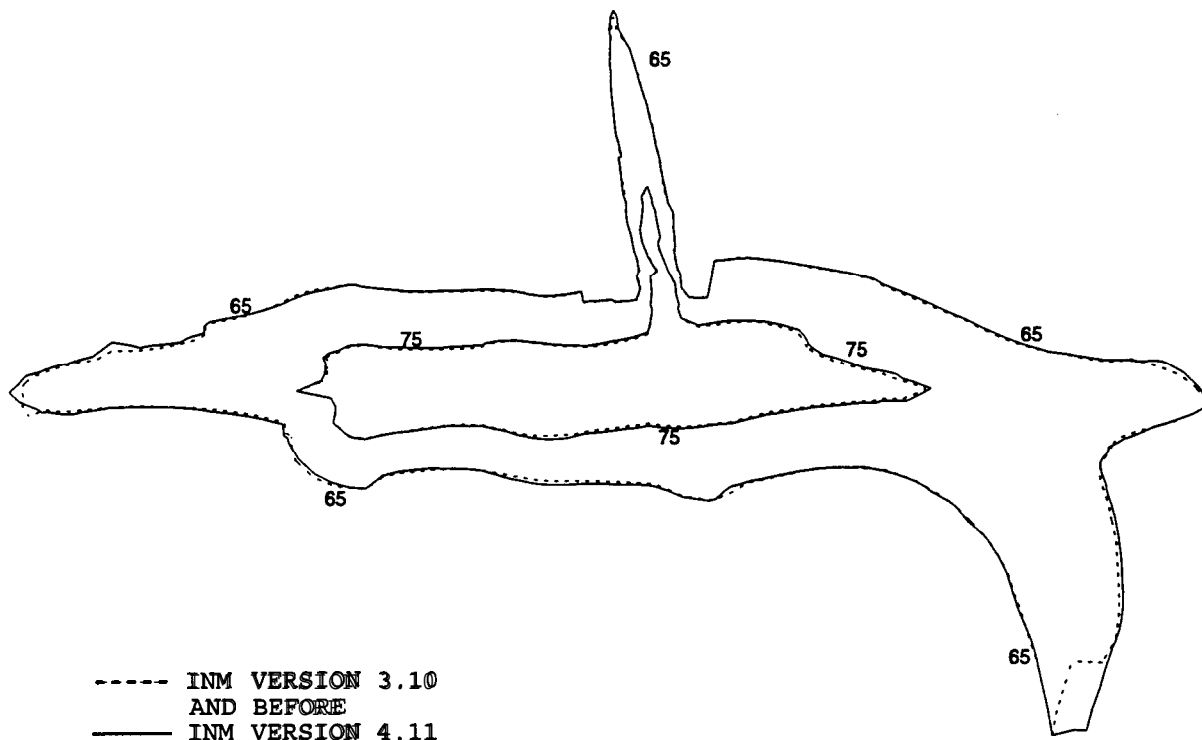


FIGURE **A-4**:: **LDN** CONTOUR COMPARISON FOR **INM** INPUT **TESTCASE**

The effect of the modified **directivity** pattern on the noise contours is depicted in Figures **A-3** and **A-4**, below. Figure **A-3** shows the effect on the **SEL** footprint for a single takeoff operation of the **B737-200** airplane (**INM** number **47**).. Figure **A-4** shows the effect on the **LDN** contour for the **INM** Input **Testcase** provided with **INM** Version **3.10**..

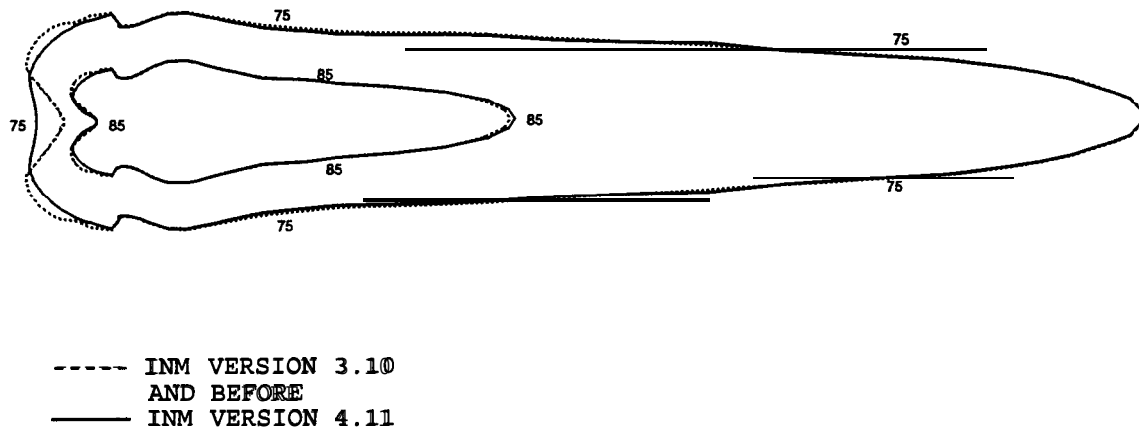


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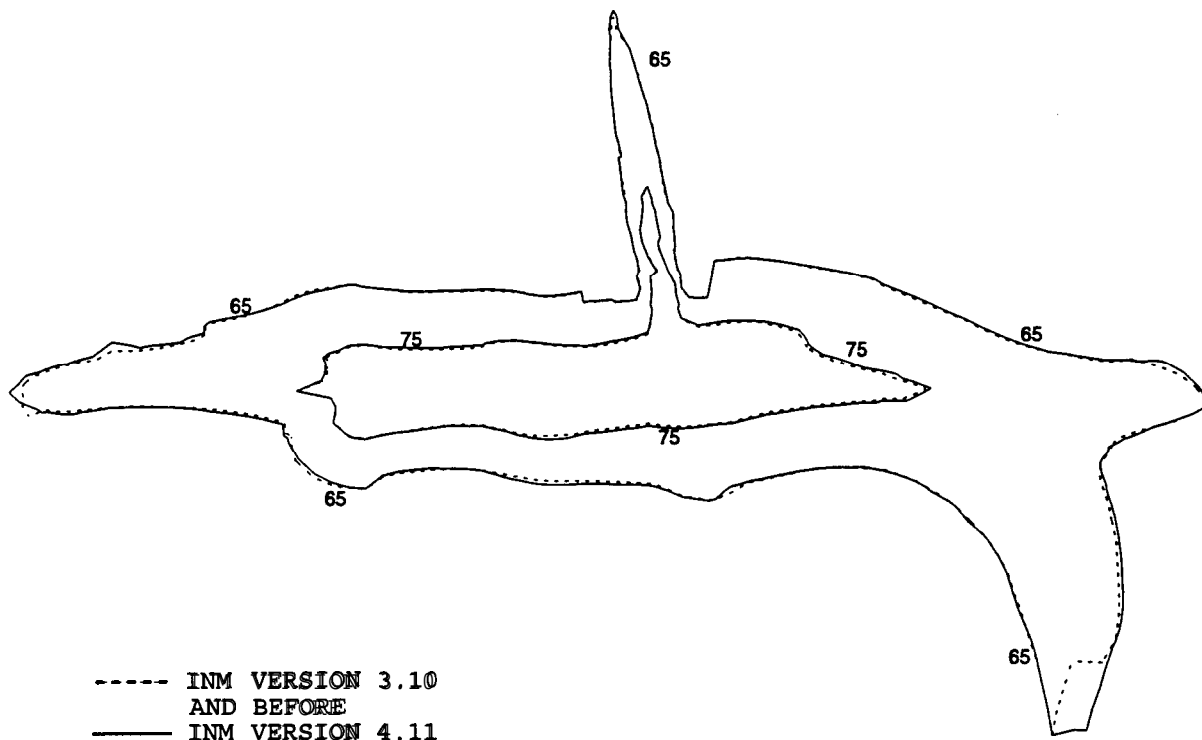


FIGURE **A-4**:: **LDN** CONTOUR COMPARISON FOR **INM** INPUT **TESTCASE**

The effect of the modified **directivity** pattern on the noise contours is depicted in Figures **A-3** and **A-4**, below. Figure **A-3** shows the effect on the **SEL** footprint for a single takeoff operation of the **B737-200** airplane (**INM** number **47**).. Figure **A-4** shows the effect on the **LDN** contour for the **INM** Input **Testcase** provided with **INM** Version **3.10**..

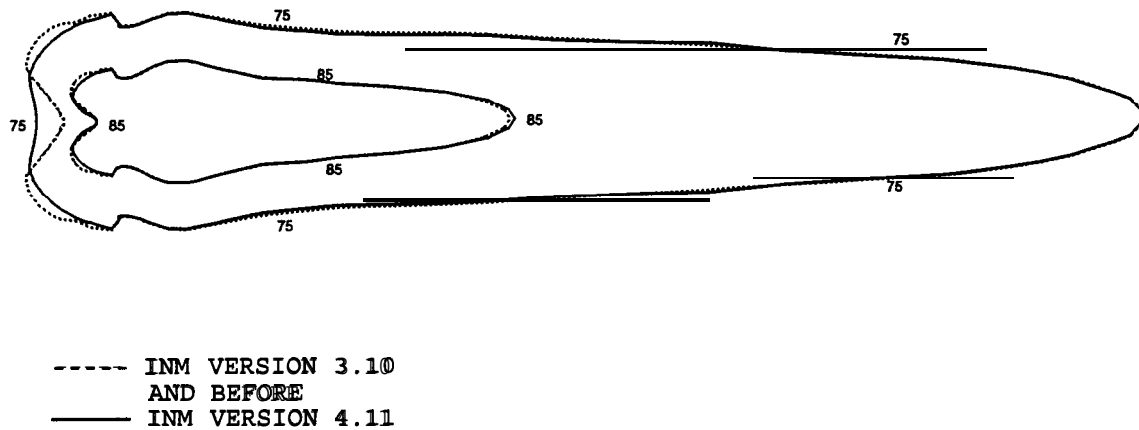


FIGURE **A-3**:: **SEL** TAKEOFF FOOTPRINT COMPARISON FOR **B737-200** AIRPLANE

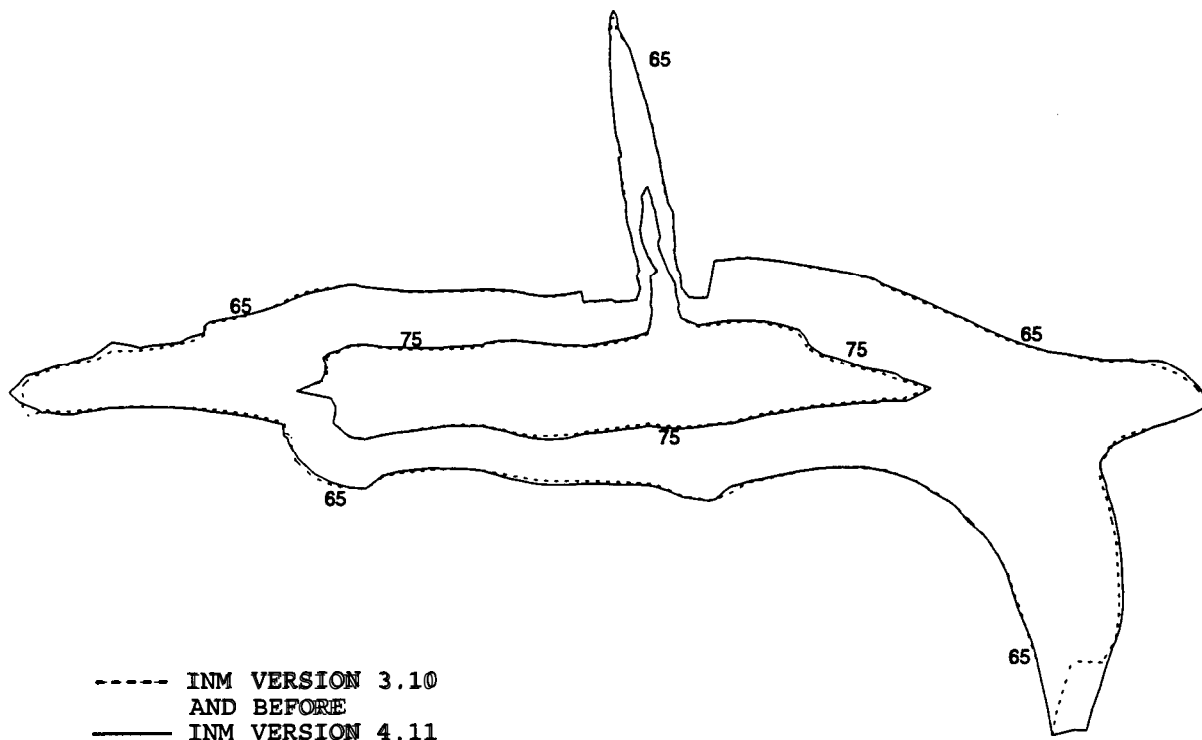


FIGURE **A-4**:: **LDN** CONTOUR COMPARISON FOR **INM** INPUT **TESTCASE**







Standard Temperature, °F:	$T_{\text{cap}} \equiv T_{\text{to}} = 59.0$
Standard Temperature, °C:	$T_{\text{cap}} \equiv T_{\text{co}} = 15.0$
Standard Temperature, °R:	$T_{\text{cap}} \equiv T_{\text{ro}} = 518.67$
Temperature Ratio:	$\text{THETA} = 1 - [(L)(H_x) / T_{\text{ro}}]$ , where $H_x$ is the altitude MSL for segment point X
Pressure Ratio:	$\text{DELTA} = \text{THETA}^{(g / ((Rc)(L)))}$
Density Ratio:	$\text{SIGMA} = \text{THETA}^{((g / ((Rc)(L))) - 1)}$
Airport Elevation MSL:	$H_{\text{ap}} = 0.0 \text{ ft}$
Brake Release Gross Weight	$= W$
Number of Engines supplying Thrust	$= N$

#### GROUND ROLL SEGMENT

For the ground roll segment the following apply:

Airport Temperature:	$T_{\text{c1}} = T_{\text{c2}} = T_{\text{cap}}$
Pressure Altitude MSL:	$H_1 = H_2 = H_{\text{ap}}$
Initial Calibrated Airspeed:	$V_{\text{c1}} = 16.0 \text{ kts}$

Given the above, the remaining parameters for the ground roll segment are computed as follows:

Initial Thrust:	$Th_1 = E + F(W_{\text{c1}}) + G_1(H_1) + G_2(H_1)^2 + H(T_{\text{c1}})$
Final Calibrated Airspeed:	$V_{\text{c2}} \equiv (C)(W)^{1/4}$
Final Airplane True Speed:	$V_{\text{t2}} \equiv V_{\text{c2}} / (\text{SIGMA})^{1/4}$
Final Thrust:	$Th_2 = E + F(W_{\text{c2}}) + G_1(H_2) + G_2(H_2)^2 + H(T_{\text{c2}})$
Segment Horizontal Length:	$S_g = [(B)(\text{THETA})(W / \text{DELTA})^2] / [(N) Th_2]$

where  $E, F, G_1, G_2,$  and  $H$  are engine-dependent coefficients from Data Base Number 11 for maximum takeoff thrust mode;

$C$  is a coefficient from Data Base Number 11 which is appropriate to the takeoff flap/slat setting;

$B$  is a coefficient from Data Base Number 11 which is appropriate to a specific airplane/flap-deflection combination, and varies only with the takeoff flap/slat setting; and

$\text{SIGMA}, \text{THETA},$  and  $\text{DELTA}$ , defined above, are constants equal to 1 at sea level..

Standard Temperature, °F:	$T_{\text{cap}} \equiv T_{\text{to}} = 59.0$
Standard Temperature, °C:	$T_{\text{cap}} \equiv T_{\text{co}} = 15.0$
Standard Temperature, °R:	$T_{\text{cap}} \equiv T_{\text{ro}} = 518.67$
Temperature Ratio:	$\text{THETA} = 1 - [(L)(H_x) / T_{\text{ro}}]$ , where $H_x$ is the altitude MSL for segment point X
Pressure Ratio:	$\text{DELTA} = \text{THETA}^{(g / ((Rc)(L)))}$
Density Ratio:	$\text{SIGMA} = \text{THETA}^{(g / ((Rc)(L)) - 1)}$
Airport Elevation MSL:	$H_{\text{ap}} = 0.0 \text{ ft}$
Brake Release Gross Weight	$= W$
Number of Engines supplying Thrust	$= N$

#### GROUND ROLL SEGMENT

For the ground roll segment the following apply:

Airport Temperature:	$T_{\text{c1}} = T_{\text{c2}} = T_{\text{cap}}$
Pressure Altitude MSL:	$H_1 = H_2 = H_{\text{ap}}$
Initial Calibrated Airspeed:	$V_{\text{c1}} = 16.0 \text{ kts}$

Given the above, the remaining parameters for the ground roll segment are computed as follows:

Initial Thrust:	$Th_1 = E + F(V_{\text{c1}}) + G_1(H_1) + G_2(H_1)^2 + H(T_{\text{c1}})$
Final Calibrated Airspeed:	$V_{\text{c2}} \equiv (C)(W)^{1/4}$
Final Airplane True Speed:	$V_{\text{t2}} \equiv V_{\text{c2}} / (\text{SIGMA})^{1/4}$
Final Thrust:	$Th_2 = E + F(V_{\text{c2}}) + G_1(H_2) + G_2(H_2)^2 + H(T_{\text{c2}})$
Segment Horizontal Length:	$S_g = [(B)(\text{THETA})(W / \text{DELTA})^2] / [(N) Th_2]$

where  $E, F, G_1, G_2,$  and  $H$  are engine-dependent coefficients from Data Base Number 11 for maximum takeoff thrust mode;

$C$  is a coefficient from Data Base Number 11 which is appropriate to the takeoff flap/slat setting;

$B$  is a coefficient from Data Base Number 11 which is appropriate to a specific airplane/flap-deflection combination, and varies only with the takeoff flap/slat setting; and

$\text{SIGMA}, \text{THETA},$  and  $\text{DELTA}$ , defined above, are constants equal to 1 at sea level..

Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

R is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

## ACCELERATION SEGMENT

For acceleration segments the following apply:

Initial Calibrated Airspeed:	$V_{c1}$	=	$V_{c2}$ of the previous segment
Initial Airplane True Speed:	$V_{t1}$	=	$V_{t2}$ of the previous segment
Initial Thrust:	$Th_1$	=	$Th_2$ of the previous segment
Initial Temperature:	$T_{c1}$	=	$T_{c2}$ of the previous segment
Initial Pressure Altitude MSL:	$H_1$	=	$H_2$ of the previous segment
Final Calibrated Airspeed:	$V_{c2}$	=	As specified in the standard flight procedure
Rate-of-Climb:	$V_{t2}$	=	As specified in the standard flight procedure

Given the above, computation of the remaining parameters is performed using an iterative procedure to arrive at the altitude increment,  $\Delta H$ . If the difference between  $\Delta H$  and  $\Delta H_c$  (the computed altitude increment for the current iteration) is greater than one ft,  $\Delta H$  is set equal to  $\Delta H_{c''}$  and the iterative process is repeated until a difference of one ft or less is achieved.

Initial Assumed Altitude Increment:	$\Delta H$	=	250 ft
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### Start of Iterative Loop:

Final Segment Altitude MSL:	$H_2$	=	$H_1 + \Delta H$
Final Segment Temperature:	$T_{c2}$	=	$\{ [T_{fap} = L(H_2)] - 32 \} (5/9)$
Final True Speed:	$V_{t2}$	=	$V_{c2} / (\text{SIGMA})^{0.4}$
Final Segment Thrust:	$Th_2$	=	$E + F(V_{c2}) + G_1(H_2) + G_2(H_2)^2 + H(T_{c2})$
Average Segment Thrust:	$Th_{avg}$	=	$0.5(Th_1 + Th_2)$
Average True Speed:	$V_{tavg}$	=	$0.5(V_{t1} + V_{t2})$

$$\begin{aligned}
\text{Average Segment Altitude:} \quad H_{\text{avg}} &= H_1 + 0.5 \Delta H \\
\text{Average Airplane Weight:} \quad W_{\text{avg}} &= W / \{ [\text{THETA}] (g/t (R) (L)) 1 \} \\
\text{Sine of the Flight Angle:} \quad \text{SIN}_{\text{ang}} &= V_{t2} / (101.2685 V_{\text{avg}}) \\
\text{Flight Angle:} \quad \text{GAMMA} &= \arcsin(\text{SIN}_{\text{ang}}) \\
\text{Horizontal Segment Distance:} \quad S_g &= \frac{0.042062 (V_{t2}^2 - V_{t1}^2)}{[ (N) (Th_{\text{avg}}) / W_{\text{avg}} ] - R_{\text{avg}} - \text{SIN}_{\text{ang}}} \\
\text{Computed Altitude Increment:} \quad \Delta H_c &= S_g [\tan(\text{GAMMA})] (1/0.95) \\
\text{Deviation of the Computed Altitude Increment from the Altitude Increment Assumed at the Start of the Current Iteration Cycle} \quad \text{DEV} &= \text{abs}[\Delta H_c - \Delta H]
\end{aligned}$$

At this point the status of the iterative process is checked. If DEV is less than 1 ft., then the iterative process is complete. Otherwise,

$$\text{Altitude Increment:} \quad \Delta H = \Delta H_c$$

and the iterative process is repeated as above.

where  $E$ ,  $F$ ,  $G_1$ ,  $G_2$ , and  $H$  are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

$R_{\text{avg}}$  is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

### THRUST REDUCTION SEGMENT

A thrust reduction segment of **1000 ft** (horizontal distance) is introduced to allow for a smooth transition of the thrust associated with the Federal Aviation Regulations, Part 36 thrust cutback point. This segment replaces the first **1000 ft** of horizontal distance of the next segment which may be either a climb or an acceleration segment. Computation of the parameters associated with the thrust reduction segment and the next segment is performed simultaneously. For the thrust reduction segment the following apply:

$$\begin{aligned}
\text{Initial Calibrated Airspeed:} \quad V_{c1} &= V_{c2} \text{ of the previous segment} \\
\text{Initial Pressure Altitude MSL:} \quad H_1 &= H_2 \text{ of the previous segment} \\
\text{Initial Temperature:} \quad T_{c1} &= T_{c2} \text{ of the previous segment}
\end{aligned}$$

$$\begin{aligned}
\text{Average Segment Altitude:} \quad H_{\text{avg}} &= H_1 + 0.5 \Delta H \\
\text{Average Airplane Weight:} \quad W_{\text{avg}} &= W / \{ [\text{THETA}] (g/t (R) (L)) \} \\
\text{Sine of the Flight Angle:} \quad \text{SIN}_{\text{ang}} &= V_{t2} / (101.2685 V_{\text{avg}}) \\
\text{Flight Angle:} \quad \text{GAMMA} &= \arcsin(\text{SIN}_{\text{ang}}) \\
\text{Horizontal Segment Distance:} \quad S_g &= \frac{0.042062 (V_{t2}^2 - V_{t1}^2)}{[(N) (Th_{\text{avg}}) / W_{\text{avg}}] - R_{\text{avg}} - \text{SIN}_{\text{ang}}} \\
\text{Computed Altitude Increment:} \quad \Delta H_c &= S_g [\tan(\text{GAMMA})] (1/0.95) \\
\text{Deviation of the Computed Altitude Increment from the Altitude Increment Assumed at the Start of the Current Iteration Cycle} \quad \text{DEV} &= \text{abs}[\Delta H_c - \Delta H]
\end{aligned}$$

At this point the status of the iterative process is checked. If DEV is less than 1 ft., then the iterative process is complete. Otherwise,

$$\text{Altitude Increment:} \quad \Delta H = \Delta H_c$$

and the iterative process is repeated as above.

where  $E$ ,  $F$ ,  $G_1$ ,  $G_2$ , and  $H$  are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

$R_{\text{avg}}$  is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

### THRUST REDUCTION SEGMENT

A thrust reduction segment of **1000 ft** (horizontal distance) is introduced to allow for a smooth transition of the thrust associated with the Federal Aviation Regulations, Part 36 thrust cutback point. This segment replaces the first **1000 ft** of horizontal distance of the next segment which may be either a climb or an acceleration segment. Computation of the parameters associated with the thrust reduction segment and the next segment is performed simultaneously. For the thrust reduction segment the following apply:

$$\begin{aligned}
\text{Initial Calibrated Airspeed:} \quad V_{c1} &= V_{c2} \text{ of the previous segment} \\
\text{Initial Pressure Altitude MSL:} \quad H_1 &= H_2 \text{ of the previous segment} \\
\text{Initial Temperature:} \quad T_{c1} &= T_{c2} \text{ of the previous segment}
\end{aligned}$$

$$\begin{aligned}
\text{Average Segment Altitude:} \quad H_{\text{avg}} &= H_1 + 0.5 \Delta H \\
\text{Average Airplane Weight:} \quad W_{\text{avg}} &= W / \{ [\text{THETA}] (g/t (R) (L)) 1 \} \\
\text{Sine of the Flight Angle:} \quad \text{SIN}_{\text{ang}} &= V_{t2} / (101.2685 V_{\text{avg}}) \\
\text{Flight Angle:} \quad \text{GAMMA} &= \arcsin(\text{SIN}_{\text{ang}}) \\
\text{Horizontal Segment Distance:} \quad S_g &= \frac{0.042062 (V_{t2}^2 - V_{t1}^2)}{[ (N) (Th_{\text{avg}}) / W_{\text{avg}} ] - R_{\text{avg}} - \text{SIN}_{\text{ang}}} \\
\text{Computed Altitude Increment:} \quad \Delta H_c &= S_g [\tan(\text{GAMMA})] (1/0.95) \\
\text{Deviation of the Computed Altitude Increment from the Altitude Increment Assumed at the Start of the Current Iteration Cycle} \quad \text{DEV} &= \text{abs}[\Delta H_c - \Delta H]
\end{aligned}$$

At this point the status of the iterative process is checked. If DEV is less than 1 ft., then the iterative process is complete. Otherwise,

$$\begin{aligned}
\text{Altitude Increment:} \quad \Delta H &= \Delta H_c
\end{aligned}$$

and the iterative process is repeated as above.

where  $E$ ,  $F$ ,  $G_1$ ,  $G_2$ , and  $H$  are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

$R_{\text{avg}}$  is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

### THRUST REDUCTION SEGMENT

A thrust reduction segment of **1000 ft** (horizontal distance) is introduced to allow for a smooth transition of the thrust associated with the Federal Aviation Regulations, Part 36 thrust cutback point. This segment replaces the first **1000 ft** of horizontal distance of the next segment which may be either a climb or an acceleration segment. Computation of the parameters associated with the thrust reduction segment and the next segment is performed simultaneously. For the thrust reduction segment the following apply:

$$\begin{aligned}
\text{Initial Calibrated Airspeed:} \quad V_{c1} &= V_{c2} \text{ of the previous segment} \\
\text{Initial Pressure Altitude MSL:} \quad H_1 &= H_2 \text{ of the previous segment} \\
\text{Initial Temperature:} \quad T_{c1} &= T_{c2} \text{ of the previous segment}
\end{aligned}$$



Non-Standard Temperature Ratio:	$\text{THETA}_{ns} =$	$\text{SIGMA}_{ns} \cdot (1/(g/(Rc)(L)-1)))$
Non-Standard Pressure Ratio:	$\text{DELTA}_{ns} =$	$\text{THETA}_{ns} \cdot (g/(Rc)(L))$

### GROUND ROLL SEGMENT

For the ground roll segment the following apply:

Airport Temperature:	$T_{c1} =$	$T_{c2} =$	$(T_{fap} - 32) (5/9)$
Pressure Altitude MSL:	$H_1 =$	$H_2 =$	$H_{ap}$
Initial Calibrated Airspeed:	$V_{c1} =$	$16.0 \text{ kts}$	

Given the above, the remaining parameters for the ground roll segment under non-standard conditions are computed as in Section **B.1**, Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

### CLIMB SEGMENT

The parameters for the climb segment under non-standard conditions are computed as in Section **B.1**, Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

### ACCELERATION SEGMENT

With the exception of the iterative process described below, the parameters for the acceleration segment under non-standard conditions are computed as in Section **B.1**, Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

Computation of the remaining parameters is performed using an iterative procedure to arrive at the horizontal distance of the segment,  $S_{gns}$ . If the difference between  $S_{gns}$  and  $S_{gc}$  (the computed horizontal distance for the current iteration) is greater than ten ft,  $S_{gns}$  is set equal to the arithmetic average of  $S_{gns}$  and  $S_{gc}$ , and the iterative process is repeated until a difference of ten ft or less is achieved.

Initial Assumed Horizontal Distance:	$S_{gns} =$	$S_g \text{ computed for standard conditions}$
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The equations for the acceleration segment under standard conditions are used to supplement the following non-standard computations:

Start of Iterative Loop:

Tangent of the Flight Angle:	$\text{TAN}_{agg} =$	$0.95 (D_{cl}/S_{gns})$
---------------------------------	----------------------	-------------------------

Sine of the  
Flight Angle:  $\text{SIN}_{\text{ang}} = \sin[\arctan((\text{ATAN}_{\text{ang}}))]1$

Computed Horizontal  
Distance: 
$$\text{S}_{\text{gc}} = \frac{(\frac{1}{2}g) (0.95) (V_{\text{LZ}}^2 - V_{\text{th}}^2)}{[N(\text{Th}_{\text{avg}})] - R_{\text{avg}} - \text{SIN}_{\text{ang}}}$$

Deviation of the  
Computed Horizontal  
Distance from the  
Horizontal Distance  
Assumed at the Start  
of the Current  
Iteration Cycle:  $\text{DEV} = \text{abs}[\text{S}_{\text{gc}} - \text{S}_{\text{gns}}]$

At this point the status of the iterative process is checked. If DEV is less than ten ft., then the iterative process is complete. Otherwise,

Horizontal  
Distance:  $\text{S}_{\text{gns}} = 0.5[\text{S}_{\text{gc}} + \text{S}_{\text{gns}}]$

and the iterative process is repeated as above..

where E, F, G<sub>1</sub>, G<sub>2</sub>, and H are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

R<sub>avg</sub> is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

## **THRUST REDUCTION SEGMENT**

The parameters for the thrust reduction segment under non-standard conditions are computed as in Section B.1., Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

## **ERROR CHECKING**

The non-standard portion of the profile generator maintains several built-in error checks which guard against the computation of improper takeoff profiles. Computation of takeoff profiles is not performed if any of the following conditions are detected:

- (1) the computed flight angle for a climb segment is zero or negative;
- (2) the computed horizontal distance for an acceleration segment is zero or negative;
- (3) the number of iterations required to compute the horizontal distance of an acceleration segment exceeds five hundred; and

Sine of the  
Flight Angle:  $\text{SIN}_{\text{ang}} = \sin[\arctan((\text{ATAN}_{\text{ang}}))]1$

Computed Horizontal  
Distance: 
$$\text{S}_{\text{gc}} = \frac{(\frac{1}{2}g) (0.95) (V_{\text{LZ}}^2 - V_{\text{th}}^2)}{[N(\text{Th}_{\text{avg}})] - R_{\text{avg}} - \text{SIN}_{\text{ang}}}$$

Deviation of the  
Computed Horizontal  
Distance from the  
Horizontal Distance  
Assumed at the Start  
of the Current  
Iteration Cycle:  $\text{DEV} = \text{abs}[\text{S}_{\text{gc}} - \text{S}_{\text{gns}}]$

At this point the status of the iterative process is checked. If DEV is less than ten ft., then the iterative process is complete. Otherwise,

Horizontal  
Distance:  $\text{S}_{\text{gns}} = 0.5[\text{S}_{\text{gc}} + \text{S}_{\text{gns}}]$

and the iterative process is repeated as above..

where E, F, G<sub>1</sub>, G<sub>2</sub>, and H are engine-dependent coefficients from Data Base Number 11 for the thrust mode defined in the standard takeoff procedure; and

R<sub>avg</sub> is a coefficient from Data Base Number 11 which is the non-dimensional ratio of the airplane's drag coefficient to lift coefficient for a given flap setting and airplane configuration. The landing gear is assumed to be retracted.

## **THRUST REDUCTION SEGMENT**

The parameters for the thrust reduction segment under non-standard conditions are computed as in Section B.1, Standard Conditions, using the non-standard THETA, SIGMA, and DELTA, as appropriate.

## **ERROR CHECKING**

The non-standard portion of the profile generator maintains several built-in error checks which guard against the computation of improper takeoff profiles. Computation of takeoff profiles is not performed if any of the following conditions are detected:

- (1) the computed flight angle for a climb segment is zero or negative;
- (2) the computed horizontal distance for an acceleration segment is zero or negative;
- (3) the number of iterations required to compute the horizontal distance of an acceleration segment exceeds five hundred; and

TABLE B-1: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE **59°F** , ELEVATION **0 FT MSL**

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	4624	5004	5400	6352	7630	9173	10579
3	3719	4057	4501	5067	6644	6871	---
4	2616	2926	3240	3752	4503	5309	6699
5	3846	4157	4481	5257	6297	7545	8679
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4193	4671	---	---
9	3279	3739	4160	4913	5992	7186	8080
10	2799	3128	3656	4424	5486	6037	---
11	2684	3034	3405	4006	4436	---	---
12	3000	3338	3879	4666	5754	6709	---
13	3705	4054	4607	5400	6483	7180	8167
14	3357	3684	4204	4956	5989	6660	7614
15	2693	3335	3959	---	---	---	---
16	3279	3739	4160	4913	5992	7186	8080
17	3705	4054	4607	5400	6483	7180	8167
18	6967	6967	8556	8556	9799	9799	---
19	3997	4389	4943	5838	6813	7868	---
20	3371	3656	3954	4609	5534	6575	7799
21	4669	5071	5463	6353	7614	9032	10657
22	5052	5383	5900	6443	7610	8883	---
23	4611	4897	5343	5811	6741	7747	8869
24	5968	6863	7821	8841	---	---	---
25	4513	5004	5522	6146	---	---	---
26	5460	6050	6913	8098	9476	---	---
27	5979	6964	8028	9074	---	---	---
28	4513	5004	5522	6146	---	---	---
29	5460	6050	6913	8098	9476	---	---
30	5263	6120	6965	7699	---	---	---
31	3352	3846	4285	5206	6369	---	---
32	3414	3703	4015	4587	5362	6268	6811
33	3020	3274	3549	4062	4765	5576	5970
34	3067	3467	3924	4411	5328	6299	---
35	3506	3981	4489	5506	---	---	---
36	3187	3681	4135	5041	---	---	---
37	4221	4827	5609	---	---	---	---
38	3292	4035	---	---	---	---	---
39	3184	3746	4612	---	---	---	---
40	3634	4416	5227	---	---	---	---
41	2124	2638	3133	---	---	---	---
42	3075	3310	3893	4618	---	---	---
43	3634	4416	5227	---	---	---	---
44	2124	2638	3133	---	---	---	---
45	3075	3310	3893	4618	---	---	---
46	3653	4186	4839	---	---	---	---
47	3303	3688	4096	4526	---	---	---
48	3897	4708	5601	---	---	---	---
49	3685	4155	4728	5991	---	---	---
50	4002	4548	5131	6493	---	---	---
51	2636	2816	3091	3573	4217	5000	5800
52	2747	2960	3219	3692	4376	5123	---
53	2826	---	---	---	---	---	---
54	2569	---	---	---	---	---	---
55	3689	---	---	---	---	---	---

TABLE B-1: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE **59°F** , ELEVATION **0 FT MSL**

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	4624	5004	5400	6352	7630	9173	10579
3	3719	4057	4501	5067	6644	6871	---
4	2616	2926	3240	3752	4503	5309	6699
5	3846	4157	4481	5257	6297	7545	8679
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4193	4671	---	---
9	3279	3739	4160	4913	5992	7186	8080
10	2799	3128	3656	4424	5486	6037	---
11	2684	3034	3405	4006	4436	---	---
12	3000	3338	3879	4666	5754	6709	---
13	3705	4054	4607	5400	6483	7180	8167
14	3357	3684	4204	4956	5989	6660	7614
15	2693	3335	3959	---	---	---	---
16	3279	3739	4160	4913	5992	7186	8080
17	3705	4054	4607	5400	6483	7180	8167
18	6967	6967	8556	8556	9799	9799	---
19	3997	4389	4943	5838	6813	7868	---
20	3371	3656	3954	4609	5534	6575	7799
21	4669	5071	5463	6353	7614	9032	10657
22	5052	5383	5900	6443	7610	8883	---
23	4611	4897	5343	5811	6741	7747	8869
24	5968	6863	7821	8841	---	---	---
25	4513	5004	5522	6146	---	---	---
26	5460	6050	6913	8098	9476	---	---
27	5979	6964	8028	9074	---	---	---
28	4513	5004	5522	6146	---	---	---
29	5460	6050	6913	8098	9476	---	---
30	5263	6120	6965	7699	---	---	---
31	3352	3846	4285	5206	6369	---	---
32	3414	3703	4015	4587	5362	6268	6811
33	3020	3274	3549	4062	4765	5576	5970
34	3067	3467	3924	4411	5328	6299	---
35	3506	3981	4489	5506	---	---	---
36	3187	3681	4135	5041	---	---	---
37	4221	4827	5609	---	---	---	---
38	3292	4035	---	---	---	---	---
39	3184	3746	4612	---	---	---	---
40	3634	4416	5227	---	---	---	---
41	2124	2638	3133	---	---	---	---
42	3075	3310	3893	4618	---	---	---
43	3634	4416	5227	---	---	---	---
44	2124	2638	3133	---	---	---	---
45	3075	3310	3893	4618	---	---	---
46	3653	4186	4839	---	---	---	---
47	3303	3688	4096	4526	---	---	---
48	3897	4708	5601	---	---	---	---
49	3685	4155	4728	5991	---	---	---
50	1002	4548	5131	6493	---	---	---
51	2646	2846	3091	3573	4217	---	---
52	2747	2960	3219	3692	4376	5123	---
53	2826	---	---	---	---	---	---
54	2569	---	---	---	---	---	---
55	3689	---	---	---	---	---	---

TABLE B-2:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 40°F , ELEVATION 0 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	4284	4603	4968	5843	7020	8439	9733
I 3	3422	I 3732	4141	4662	6112	6322	---
4	2406	2692	2981	3451	4142	4884	6163
5	3538	3824	4122	4837	5793	6942	7984
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4193	4671	---	---
9	3017	3440	3827	4520	5512	6611	7434
10	2799	3128	3656	4424	5486	6037	---
11	2470	2791	3133	3886	4881	---	---
12	2760	3070	3569	4293	5294	6172	---
13	3409	3729	4238	4968	5964	6606	7514
14	3088	3389	3868	4559	5510	6127	7005
15	2478	3068	3642	---	---	---	---
16	3017	3440	3827	4520	5512	6611	7434
17	3409	3729	4238	4968	5964	6606	7514
18	6410	6410	7872	7872	9015	9015	---
19	3677	4038	4547	5371	6268	7239	---
20	3101	3364	3638	4240	5091	6049	7175
21	4293	4666	5025	5844	7005	8309	9804
22	4648	4932	5428	5928	7001	8172	---
23	4242	4505	4916	5346	6202	7127	8199
24	5968	6863	7821	8871	---	---	---
I 25	159	I 4604	5090	5689	---	---	---
26	5023	5566	6360	7490	8718	---	---
27	5900	6407	7386	8347	---	---	---
28	4132	4604	5080	5654	---	---	---
29	5023	5566	6360	7490	8718	---	---
30	4942	5630	6408	7083	---	---	---
I 31	1084	I 1836	3942	4780	5960	---	---
32	3141	3407	3694	4220	4933	5767	6266
33	2778	3012	3265	3737	4384	5130	5492
34	2822	3189	3610	4058	4902	5795	---
35	3226	3663	4130	5065	---	---	---
36	2928	3382	3799	4631	---	---	---
37	3083	4440	5160	---	---	---	---
38	3029	3712	---	---	---	---	---
39	2930	3446	4243	---	---	---	---
40	3343	4062	4809	---	---	---	---
41	1954	2427	2883	---	---	---	---
42	2829	3045	3581	4249	---	---	---
43	3343	4062	4809	---	---	---	---
44	1954	2427	2883	---	---	---	---
45	2829	3045	3581	4249	---	---	---
46	3361	3851	4452	---	---	---	---
47 I - -	1039	3393	3788	4184	---	---	---
48	3583	4332	5153	---	---	---	---
49	3390	3822	4349	5012	---	---	---
50	3681	4184	4720	5974	---	---	---
51	2434	2619	2843	3287	3879	---	---
52	2826	2722	2961	3395	4024	4712	---
53	2600	---	---	---	---	---	---
54	2364	---	---	---	---	---	---
55	3394	---	---	---	---	---	---

TABLE B-2:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 40°F , ELEVATION 0 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
I 2	4254	4603	4968	5843	7820	8439	9733
I 1	3422	I 3732	4141	4662	6112	6322	---
4	2406	2692	2981	3451	4142	4884	6163
5	3538	3824	4122	4837	5793	6942	7984
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4193	4671	---	---
9	3017	3440	3827	4520	5512	6611	7434
10	2799	3128	3656	4424	5486	6037	---
11	2470	2791	3133	3886	4881	---	---
12	2760	3070	3569	4293	5294	6172	---
13	3409	3729	4238	4968	5964	6606	7514
14	3088	3389	3868	4559	5510	6127	7005
15	2478	3068	3642	---	---	---	---
16	3017	3440	3827	4520	5512	6611	7434
17	3409	3729	4238	4968	5964	6606	7514
18	6410	6410	7872	7872	9015	9015	---
19	3677	4038	4547	5371	6268	7239	---
20	3101	3364	3638	4240	5091	6049	7175
21	4295	4666	5026	5844	7005	8309	9804
22	4648	4952	5428	5928	7001	8172	---
23	4242	4505	4916	5346	6202	7127	8159
24	9968	6863	7821	8841	---	---	---
I 25	159	I 4604	5090	5889	---	---	---
26	5023	5566	6360	7450	8718	---	---
27	5500	6407	7386	8347	---	---	---
28	4152	4604	5080	5654	---	---	---
29	5023	5566	6360	7450	8718	---	---
30	4342	5630	6408	7083	---	---	---
I 31	1084	I 1836	3942	4780	5880	---	---
32	3141	3407	3694	4220	4933	5767	6266
33	2778	3012	3265	3737	4384	5130	5492
34	2822	3189	3610	4058	4902	5795	---
35	3226	3663	4130	5065	---	---	---
36	2928	3382	3799	4631	---	---	---
37	3013	4440	5160	---	---	---	---
38	3029	3712	---	---	---	---	---
39	2930	3446	4143	---	---	---	---
40	3343	4062	4809	---	---	---	---
41	1954	2427	2883	---	---	---	---
42	2829	3045	3581	4249	---	---	---
43	3343	4062	4809	---	---	---	---
44	1954	2427	2883	---	---	---	---
45	2829	3045	3581	4249	---	---	---
46	3361	3851	4452	---	---	---	---
47 I - -	,039	3393	3788	4184	---	---	---
48	3585	4332	5153	---	---	---	---
49	3390	3822	4349	5012	---	---	---
50	3681	4184	4720	5974	---	---	---
51	2434	2619	2843	3287	3879	---	---
52	2826	2722	2961	3395	4024	4712	---
53	2600	---	---	---	---	---	---
54	2364	---	---	---	---	---	---
55	3394	---	---	---	---	---	---

TABLE B-3:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 80°F , ELEVATION 0 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	5053	5468	5901	6941	8338	10024	11561
3	4054	4433	4919	5937	7260	7509	---
4	2858	3198	3541	4100	4920	5801	7321
5	4202	4542	4896	5745	6881	8245	9494
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3923	4193	4671	---	---
9	3583	4086	4545	5369	6548	7852	8830
10	2799	3128	3656	4424	5486	6037	---
11	2933	3305	3721	4378	4847	---	---
12	3278	3647	4239	5099	6288	7332	---
13	4049	4430	5034	5901	7084	7846	8925
14	---	---	---	---	---	---	---
15	2943	3544	4326	5415	6511	7227	8320
16	3583	4086	4545	5369	6548	7852	8830
17	4049	4430	5034	5901	7084	7846	8925
18	7614	7614	9350	9350	10708	10708	---
19	4368	4797	5401	6380	7445	8598	---
20	3683	3995	4321	5037	6047	7185	8523
21	5102	5542	5970	6942	8321	9870	11646
22	5921	6882	8447	7041	8315	9707	---
23	9039	5351	5839	6350	7306	8465	9692
24	5968	6863	7821	8841	---	---	---
25	4932	5468	6034	6716	---	---	---
26	5967	6612	7554	8849	10355	---	---
27	6933	7610	8773	9915	---	---	---
28	4932	5468	6034	6716	---	---	---
29	5967	6612	7554	8849	10355	---	---
30	5751	6688	7611	8413	---	---	---
31	3663	4283	4683	5689	6960	---	---
32	3731	4047	4387	5012	5860	6850	7443
33	3300	3578	3878	4439	5207	6094	6924
34	3332	3788	4287	4820	5823	6883	---
35	3832	4351	4905	6016	---	---	---
36	3488	4029	4526	5516	---	---	---
37	4613	5274	6129	---	---	---	---
38	3998	4409	---	---	---	---	---
39	3400	4093	5040	---	---	---	---
40	3971	4825	5712	---	---	---	---
41	2321	2883	3424	---	---	---	---
42	3361	3617	4254	5047	---	---	---
43	3971	4825	5712	---	---	---	---
44	2321	2883	3424	---	---	---	---
45	3361	3617	4254	5047	---	---	---
46	3992	4574	5288	---	---	---	---
47	3609	4030	4476	4946	---	---	---
48	4258	5145	6121	---	---	---	---
49	4027	4540	5166	6547	---	---	---
50	4373	4970	5607	7095	---	---	---
51	2891	3111	3377	3904	4608	---	---
52	3002	3236	3519	4036	4783	5600	---
53	3088	---	---	---	---	---	---
54	2808	---	---	---	---	---	---
55	4031	---	---	---	---	---	---



TABLE B-3:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 80°F , ELEVATION 0 FT MSL (CONTINUED)

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
56	4136	---	---	---	---	---	---
57	3421	---	---	---	---	---	---
58	3823	---	---	---	---	---	---
59	4071	---	---	---	---	---	---
60	3248	---	---	---	---	---	---
61	5404	---	---	---	---	---	---
62	4260	---	---	---	---	---	---
63	3006	3787	5111	---	---	---	---
64	1961	---	---	---	---	---	---
65	1850	---	---	---	---	---	---
66	4302	5485	6558	---	---	---	---
67	2941	---	---	---	---	---	---
68	2853	---	---	---	---	---	---
69	1381	---	---	---	---	---	---
70	3546	4683	6014	---	---	---	---
71	3694	2069	0	---	---	---	---
72	1997	2599	---	---	---	---	---
73	2321	---	---	---	---	---	---
74	704	---	---	---	---	---	---
75	823	---	---	---	---	---	---
76	1766	---	---	---	---	---	---
77	780	---	---	---	---	---	---
78	11509	---	---	---	---	---	---
79	4538	7077	---	---	---	---	---
80	5637	7720	---	---	---	---	---
I 81	5022	7504	---	---	---	---	---
82	5707	8528	---	---	---	---	---
83	4118	4582	4973	5806	6945	8590	9984
84	4463	4831	5197	6109	7334	8799	10152
85	3996	4646	5169	6304	---	---	---
86	3901	4508	5066	6182	---	---	---
87	3009	3262	3537	4052	4754	5569	5963
88	3215	3943	4754	---	---	---	---
89	3633	4464	5268	---	---	---	---
90	3483	4255	5112	---	---	---	---
91	12306	---	---	---	---	---	---
92	10171	---	---	---	---	---	---
93	3544	3929	4493	5267	6169	---	---
94	3283	3640	4017	4472	---	---	---
95	3346	---	---	---	---	---	---
96	4579	---	---	---	---	---	---
97	3978	4733	5637	6539	---	---	---
98	4520	---	---	---	---	---	---
99	2652	---	---	---	---	---	---
100	4513	5004	5522	6146	---	---	---
101	5460	6050	6913	8098	9476	---	---
102	4777	5163	5964	6983	7831	9004	10667
103	5189	5613	6055	7156	8358	9858	11708
104	3000	---	---	---	---	---	---
105	3000	---	---	---	---	---	---
106	3000	---	---	---	---	---	---
107	3000	---	---	---	---	---	---

TABLE B-3:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 80°F , ELEVATION 0 FT MSL (CONTINUED)

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
56	4136	---	---	---	---	---	---
57	3421	---	---	---	---	---	---
58	3823	---	---	---	---	---	---
59	4071	---	---	---	---	---	---
60	3248	---	---	---	---	---	---
61	5404	---	---	---	---	---	---
62	4260	---	---	---	---	---	---
63	3006	3787	5111	---	---	---	---
64	1961	---	---	---	---	---	---
65	1850	---	---	---	---	---	---
66	4302	5485	6558	---	---	---	---
67	2941	---	---	---	---	---	---
68	2853	---	---	---	---	---	---
69	1381	---	---	---	---	---	---
70	3546	4683	6014	---	---	---	---
71	1694	2069	0	---	---	---	---
72	1997	2599	---	---	---	---	---
73	2321	---	---	---	---	---	---
74	704	---	---	---	---	---	---
75	823	---	---	---	---	---	---
76	1766	---	---	---	---	---	---
77	780	---	---	---	---	---	---
78	11509	---	---	---	---	---	---
79	4538	7077	---	---	---	---	---
80	5637	7720	---	---	---	---	---
I 81	5022	7504	---	---	---	---	---
82	5707	8528	---	---	---	---	---
83	4118	4582	4973	5806	6945	8590	9984
84	4463	4831	5197	6109	7334	8799	10152
85	3996	4646	5169	6304	---	---	---
86	3901	4508	5066	6182	---	---	---
87	3009	3262	3537	4052	4754	5569	5963
88	3215	3943	4754	---	---	---	---
89	3633	4454	5268	---	---	---	---
90	3483	4255	5112	---	---	---	---
91	12306	---	---	---	---	---	---
92	10171	---	---	---	---	---	---
93	3544	3929	4493	5267	6169	---	---
94	3283	3640	4017	4472	---	---	---
95	3346	---	---	---	---	---	---
96	4579	---	---	---	---	---	---
97	3978	4733	5637	6539	---	---	---
98	4520	---	---	---	---	---	---
99	2652	---	---	---	---	---	---
100	4513	5004	5522	6146	---	---	---
101	5460	6050	6913	8098	9476	---	---
102	4797	5163	5564	6563	7651	9004	20667
103	5189	5613	6055	7156	8358	9858	11708
104	3000	---	---	---	---	---	---
105	3000	---	---	---	---	---	---
106	3000	---	---	---	---	---	---
107	3000	---	---	---	---	---	---

TABLE B-4: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 59°F , ELEVATION 3000 FT MSL (CONTINUED)

LINE #	STAGE WEIGHT						
	1	2	3	4	5	6	7
56	4136	---	---	---	---	---	---
57	3647	---	---	---	---	---	---
58	4240	---	---	---	---	---	---
59	4790	---	---	---	---	---	---
60	3458	---	---	---	---	---	---
I 61	5994	---	---	---	---	---	---
62	4793	---	---	---	---	---	---
63	3261	4108	5545	---	---	---	---
64	2156	---	---	---	---	---	---
65	1464	---	---	---	---	---	---
66	4667	5951	7115	---	---	---	---
67	3191	---	---	---	---	---	---
68	3095	---	---	---	---	---	---
69	1499	---	---	---	---	---	---
70	3847	5081	6525	---	---	---	---
71	1838	2245	0	---	---	---	---
72	2167	2820	---	---	---	---	---
73	2518	---	---	---	---	---	---
74	764	---	---	---	---	---	---
I 75	483	---	---	---	---	---	---
76	1916	---	---	---	---	---	---
77	846	---	---	---	---	---	---
78	13454	---	---	---	---	---	---
79	5094	7944	---	---	---	---	---
80	6328	8665	---	---	---	---	---
81	5448	8141	---	---	---	---	---
82	6192	9252	---	---	---	---	---
83	4637	5160	5599	6535	7015	9662	11228
84	5045	5455	5872	6900	8281	9832	10657
85	4503	5235	5823	7099	---	---	---
I 86	4233	I 4890	5494	6693	---	---	---
87	3464	3755	4071	4664	5471	6408	6861
88	3717	0	0	---	---	---	---
89	3949	4349	5718	---	---	---	---
90	4008	4896	5881	---	---	---	---
91	13820	---	---	---	---	---	---
92	11445	---	---	---	---	---	---
93	4029	4466	5106	5905	7008	---	---
94	3800	4214	4650	5176	---	---	---
I 95	3660	---	---	---	---	---	---
96	5268	---	---	---	---	---	---
97	4693	5591	6659	7725	---	---	---
98	5066	---	---	---	---	---	---
99	2913	---	---	---	---	---	---
100	4513	5004	5522	6146	---	---	---
101	5460	6050	6913	8098	9476	---	---
102	4968	5367	5783	6816	7939	9335	11051
103	5183	5603	6041	7131	8318	9796	11616
104	3000	---	---	---	---	---	---
105	3000	---	---	---	---	---	---
106	3000	---	---	---	---	---	---
107	3000	---	---	---	---	---	---

TABLE B-4: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 59°F , ELEVATION 3000 FT MSL (CONTINUED)

LINE #	STAGE WEIGHT						
	1	2	3	4	5	6	7
56	4136	---	---	---	---	---	---
57	3647	---	---	---	---	---	---
58	4240	---	---	---	---	---	---
59	4790	---	---	---	---	---	---
60	3458	---	---	---	---	---	---
I 61	5994	---	---	---	---	---	---
62	4799	---	---	---	---	---	---
63	3261	4108	9545	---	---	---	---
64	2156	---	---	---	---	---	---
65	1463	---	---	---	---	---	---
66	4667	9951	7135	---	---	---	---
67	3191	---	---	---	---	---	---
68	3085	---	---	---	---	---	---
69	3499	---	---	---	---	---	---
70	3847	9081	6525	---	---	---	---
71	3838	2245	0	---	---	---	---
72	2167	2820	---	---	---	---	---
73	2930 2518	---	---	---	---	---	---
74	764	---	---	---	---	---	---
I 75	903	---	---	---	---	---	---
I 76	1916	---	---	---	---	---	---
77	846	---	---	---	---	---	---
78	13454	---	---	---	---	---	---
79	5094	7944	---	---	---	---	---
80	6328	8665	---	---	---	---	---
81	9448	8143	---	---	---	---	---
82	6192 6137	9252	---	---	---	---	---
83	4337	5160	9599	6935	7015	9662	11220
84	5043	5459	5872	6900	8281	9932	11457
85	4303	5235	5823	7099	---	---	---
I 86	4233	I 4890	9044	8698	---	---	---
87	3464	3755	4071	4664	5471	6408	6861
88	3717	0	0	---	---	---	---
89	3949	4849	5718	---	---	---	---
90	4008	4896	5881	---	---	---	---
91	13820	---	---	---	---	---	---
92	11445	---	---	---	---	---	---
93	4029	4468	5106	5905	7008	---	---
94	3000 3000	4214	4690	5176	---	---	---
I 95	3000	---	---	---	---	---	---
I 96	5708	---	---	---	---	---	---
97	4698	5591	6659	7725	---	---	---
98	5066	---	---	---	---	---	---
99	2913	---	---	---	---	---	---
100	4513	5004	5522	6146	---	---	---
101	5460	6050	6913	8098	9476	---	---
102	4968	5367	5783	6816	7939	9335	11051
103	5183	5603	6041	7131	8318	9796	11616
104	3000	---	---	---	---	---	---
105	3000	---	---	---	---	---	---
106	3000	---	---	---	---	---	---
107	3000	---	---	---	---	---	---

**TABLE B-5: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 40°F , ELEVATION 3000 FT MSL (CONTINUED)**

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
56	4136	---	---	---	---	---	---
57	3355	---	---	---	---	---	---
58	3901	---	---	---	---	---	---
59	4407	---	---	---	---	---	---
60	3181	---	---	---	---	---	---
61	5514	---	---	---	---	---	---
62	4414	---	---	---	---	---	---
63	2945	3710	5007	---	---	---	---
64	---	---	---	---	---	---	---
65	1322	---	---	---	---	---	---
66	4204	5373	6124	---	---	---	---
67	2881	---	---	---	---	---	---
68	2795	---	---	---	---	---	---
69	1353	---	---	---	---	---	---
70	3474	4588	5892	---	---	---	---
71	1660	2027	0	---	---	---	---
72	1957	2546	---	---	---	---	---
73	2274	---	---	---	---	---	---
74	690	---	---	---	---	---	---
75	806	---	---	---	---	---	---
76	1730	---	---	---	---	---	---
77	764	---	---	---	---	---	---
78	12377	---	---	---	---	---	---
79	4886	7308	---	---	---	---	---
80	5822	7972	---	---	---	---	---
81	4320	7351	---	---	---	---	---
82	5591	8354	---	---	---	---	---
83	4266	4747	5151	6012	7189	8889	10329
84	4639	5022	5402	6348	7618	9137	10540
85	4343	4816	5357	6533	---	---	---
86	3895	4499	5054	6162	---	---	---
87	3186	3455	3745	4290	5033	5895	6312
88	3420	4193	0	---	---	---	---
89	3633	4161	5261	---	---	---	---
90	3697	4505	5411	---	---	---	---
91	12695	---	---	---	---	---	---
92	10529	---	---	---	---	---	---
93	3706	4108	4697	5506	6448	---	---
94	3496	3877	4278	4762	---	---	---
95	3367	---	---	---	---	---	---
96	4846	---	---	---	---	---	---
97	4322	5143	6126	7107	---	---	---
98	4661	---	---	---	---	---	---
99	2680	---	---	---	---	---	---
100	4513	5004	5522	6146	---	---	---
101	5460	6050	6913	8098	9476	---	---
102	4224	4563	4915	5790	6742	7923	9374
103	4333	4683	5047	5953	6939	8166	9675
104	3000	---	---	---	---	---	---
105	3000	---	---	---	---	---	---
106	3000	---	---	---	---	---	---
107	3000	---	---	---	---	---	---

TABLE B-6:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 80°F , ELEVATION 3000 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	6283	6799	7336	8628	10362	12453	14358
3	5056	5514	6117	6885	9023	9332	---
4	3557	3979	4405	5100	6120	7213	9099
5	5126	5540	5971	7003	8385	10044	11549
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4193	4671	---	---
9	4402	5020	5583	6592	8037	9636	10833
10	2799	3128	3656	4424	5486	6037	---
11	3637	4110	4613	5426	6007	---	---
12	4205	4678	5438	6541	8066	9405	---
13	5189	5677	6452	7563	9079	10056	11438
14	4519	4958	5658	6667	8055	8955	10236
15	3718	0	0	---	---	---	---
16	4402	5020	5583	6592	8037	9636	10833
17	5189	5677	6452	7563	9079	10056	11438
18	9489	9489	11650	11650	13340	13340	---
19	5638	6192	6973	8237	9613	11102	---
20	4513	4895	5293	6168	7403	8794	10428
21	6558	7123	7673	8924	10696	12688	14971
22	6846	7293	7993	8728	10304	12025	---
23	6277	6665	7272	7908	9171	10537	12062
24	5968	6863	7821	8841	---	---	---
25	6363	7056	7785	8666	---	---	---
26	7382	8179	9344	10944	12805	---	---
27	8377	9758	11249	12713	---	---	---
28	6363	7056	7785	8666	---	---	---
29	7382	8179	9344	10944	12805	---	---
30	7126	8286	9429	10422	---	---	---
31	4725	5422	6041	7339	8980	---	---
32	4585	4973	5390	6157	7196	8409	9136
33	3940	4272	4629	5297	6211	7265	7777
34	3939	4450	5034	5657	6829	8068	---
35	4545	5159	5814	7125	---	---	---
36	4297	4962	5573	6792	---	---	---
37	5931	6782	7881	---	---	---	---
38	4260	5464	---	---	---	---	---
39	4333	5096	6274	---	---	---	---
40	5082	6176	7311	---	---	---	---
41	2964	3681	4372	---	---	---	---
42	4324	4654	5473	6494	---	---	---
43	5082	6176	7311	---	---	---	---
44	2964	3681	4372	---	---	---	---
45	4324	4654	5473	6494	---	---	---
46	5108	5852	6766	---	---	---	---
47	4473	4995	5547	6129	---	---	---
48	5240	6330	7528	---	---	---	---
49	4970	5603	6375	8076	---	---	---
50	5495	6245	7045	8914	---	---	---
51	3561	3831	4159	4807	5672	---	---
52	3593	3871	4210	4825	5716	6689	---
53	3690	---	---	---	---	---	---
54	3586	---	---	---	---	---	---
55	5212	---	---	---	---	---	---

TABLE B-6:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 80°F , ELEVATION 3000 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	6283	6799	7336	8628	10362	12453	14358
3	5066	5511	6117	6885	8023	9332	---
4	3557	3979	4405	5100	6120	7213	9099
5	5126	5540	5971	7003	8385	10044	11549
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4193	4671	---	---
9	4402	5020	5583	6592	8037	9636	10833
10	2799	3128	3656	4424	5486	6037	---
11	3637	4110	4613	5426	6007	---	---
12	4205	4678	5438	6541	8066	9405	---
13	5189	5677	6452	7563	9079	10056	11438
14	4519	4958	5658	6667	8055	8955	10236
15	3718	0	0	---	---	---	---
16	4402	5020	5583	6592	8037	9636	10833
17	5189	5677	6452	7563	9079	10056	11438
18	9489	9489	11650	11650	13340	13340	---
19	5638	6192	6973	8237	9613	11102	---
20	4513	4895	5293	6168	7403	8794	10428
21	6558	7123	7673	8924	10696	12688	14971
22	6846	7293	7993	8728	10304	12025	---
23	6277	6665	7272	7908	9171	10537	12062
24	5968	6863	7821	8841	---	---	---
25	6363	7056	7785	8666	---	---	---
26	7382	8179	9344	10944	12805	---	---
27	8377	9758	11249	12713	---	---	---
28	6363	7056	7785	8666	---	---	---
29	7382	8179	9344	10944	12805	---	---
30	7126	8286	9429	10422	---	---	---
31	4725	5422	6041	7339	8980	---	---
32	4585	4973	5390	6157	7196	8409	9136
33	3940	4272	4629	5297	6211	7265	7777
34	3939	4450	5034	5657	6829	8068	---
35	4545	5159	5814	7125	---	---	---
36	4297	4962	5573	6792	---	---	---
37	5931	6782	7881	---	---	---	---
38	4160	5464	---	---	---	---	---
39	4113	5096	6274	---	---	---	---
40	5082	6176	7311	---	---	---	---
41	2964	3681	4372	---	---	---	---
42	4324	4654	5473	6494	---	---	---
43	5082	6176	7311	---	---	---	---
44	2964	3681	4372	---	---	---	---
45	4324	4654	5473	6494	---	---	---
46	5108	5852	6766	---	---	---	---
47	4473	4995	5547	6129	---	---	---
48	5240	6330	7528	---	---	---	---
49	4970	5603	6375	8076	---	---	---
50	5495	6245	7045	8914	---	---	---
51	3561	3831	4159	4807	5672	---	---
52	3593	3871	4210	4825	5716	6689	---
53	3690	---	---	---	---	---	---
54	3586	---	---	---	---	---	---
55	5212	---	---	---	---	---	---

TABLE B-6:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 80°F , ELEVATION 3000 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	6283	6799	7336	8628	10362	12453	14358
3	5066	5511	6117	6885	9023	9332	---
4	3557	3979	4405	5100	6120	7213	9099
5	5126	5540	5971	7003	8385	10044	11549
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4193	4671	---	---
9	4402	5020	5583	6592	8037	9636	10833
10	2799	3128	3656	4424	5486	6037	---
11	3637	4110	4613	5426	6007	---	---
12	4205	4678	5438	6541	8066	9405	---
13	5189	5677	6452	7563	9079	10056	11438
14	4519	4958	5658	6667	8055	8955	10236
15	3718	0	0	---	---	---	---
16	4402	5020	5583	6592	8037	9636	10833
17	5189	5677	6452	7563	9079	10056	11438
18	9489	9489	11650	11650	13340	13340	---
19	5638	6192	6973	8237	9613	11102	---
20	4513	4895	5293	6168	7403	8794	10428
21	6558	7123	7673	8924	10696	12688	14971
22	6846	7293	7993	8728	10304	12025	---
23	6277	6665	7272	7908	9171	10537	12062
24	5968	6863	7821	8841	---	---	---
25	6363	7056	7785	8666	---	---	---
26	7382	8179	9344	10944	12805	---	---
27	8377	9758	11249	12713	---	---	---
28	6363	7056	7785	8666	---	---	---
29	7382	8179	9344	10944	12805	---	---
30	7126	8286	9429	10422	---	---	---
31	4725	5422	6041	7339	8980	---	---
32	4585	4973	5390	6157	7196	8409	9136
33	3940	4272	4629	5297	6211	7265	7777
34	3939	4450	5034	5657	6829	8068	---
35	4545	5159	5814	7125	---	---	---
36	4297	4962	5573	6792	---	---	---
37	5931	6782	7881	---	---	---	---
38	4480	5464	---	---	---	---	---
39	4333	5096	6274	---	---	---	---
40	5082	6176	7311	---	---	---	---
41	2964	3681	4372	---	---	---	---
42	4324	4654	5473	6494	---	---	---
43	5082	6176	7311	---	---	---	---
44	2964	3681	4372	---	---	---	---
45	4324	4654	5473	6494	---	---	---
46	5108	5852	6766	---	---	---	---
47	4473	4995	5547	6129	---	---	---
48	5240	6330	7528	---	---	---	---
49	4970	5603	6375	8076	---	---	---
50	5495	6245	7045	8914	---	---	---
51	3561	3831	4159	4807	5672	---	---
52	3593	3871	4210	4825	5716	6689	---
53	3690	---	---	---	---	---	---
54	3586	---	---	---	---	---	---
55	5212	---	---	---	---	---	---



TABLE B-7:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 59°F , ELEVATION 6000 FT MSL (CONTINUED)

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
56	4136	---	---	---	---	---	---
57	4399	---	---	---	---	---	---
58	5180	---	---	---	---	---	---
59	6192	---	---	---	---	---	---
60	4168	---	---	---	---	---	---
61	7322	---	---	---	---	---	---
62	6054	---	---	---	---	---	---
63	3960	4989	6733	---	---	---	---
64	2613	---	---	---	---	---	---
65	1778	---	---	---	---	---	---
66	5667	7225	8639	---	---	---	---
67	3874	---	---	---	---	---	---
68	3758	---	---	---	---	---	---
69	1820	---	---	---	---	---	---
70	4672	6169	7923	---	---	---	---
71	2232	2726	0	---	---	---	---
72	2631	3424	---	---	---	---	---
73	3057	---	---	---	---	---	---
74	928	---	---	---	---	---	---
75	1084	---	---	---	---	---	---
76	2327	---	---	---	---	---	---
77	1027	---	---	---	---	---	---
78	17276	---	---	---	---	---	---
79	6260	9762	---	---	---	---	---
80	7779	10648	---	---	---	---	---
81	6616	9885	---	---	---	---	---
82	7519	11234	---	---	---	---	---
83	5744	6391	6934	8092	9673	11956	13889
84	6267	6783	7296	8571	10283	12329	14218
85	5582	6488	7215	8794	---	---	---
86	5073	5858	6578	8016	---	---	---
87	4381	4749	5148	5897	6918	8101	8674
88	0	0	0	---	---	---	---
89	4739	5815	6854	---	---	---	---
90	5068	6190	7434	---	---	---	---
91	17102	---	---	---	---	---	---
92	14072	---	---	---	---	---	---
93	5034	5580	6378	7475	8753	---	---
94	4833	5359	5913	6582	---	---	---
95	4448	---	---	---	---	---	---
96	6659	---	---	---	---	---	---
97	6095	7253	8639	10023	---	---	---
98	6323	---	---	---	---	---	---
99	3528	---	---	---	---	---	---
100	4513	5004	5522	6146	---	---	---
101	5460	6050	6913	8098	9476	---	---
102	6256	6758	7281	8581	9994	11750	13906
103	6435	6955	7498	8848	10319	12149	14402
104	3000	---	---	---	---	---	---
105	3000	---	---	---	---	---	---
106	3000	---	---	---	---	---	---
107	3000	---	---	---	---	---	---

TABLE B-8: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 40°F , ELEVATION 6000 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	6652	7197	7766	9131	10964	13173	15186
3	5354	5838	6476	7288	9549	9876	---
4	3768	4215	4666	5400	6479	7636	9630
5	5302	5729	6174	7240	8665	10376	11928
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4053	4671	---	---
9	4553	5190	5772	6813	8304	9952	11187
10	2799	3128	3656	4424	5486	6037	---
11	3811	4305	4832	5682	6290	---	---
12	4564	5078	5902	7100	8756	10210	---
13	5627	6157	6997	8202	9846	10906	12405
14	4718	5175	5904	6956	8401	9338	10671
15	0	0	0	---	---	---	---
16	4553	5190	5772	6813	8304	9952	11187
17	5627	6157	6997	8202	9846	10906	12405
18	10014	10014	12293	12293	14074	14074	---
19	6158	6763	7616	8997	10501	12129	---
20	4687	5083	5496	6404	7684	9124	10817
21	7132	7748	8346	9706	11634	13801	16285
22	7182	7650	8383	9152	10801	12602	---
23	6614	7023	7661	8330	9659	11096	12698
24	5968	6863	7821	8841	---	---	---
25	6885	7634	8423	9376	---	---	---
26	8030	8898	10165	11906	13930	---	---
27	9155	10665	12295	13896	---	---	---
28	6885	7634	8423	9376	---	---	---
29	8030	8898	10165	11906	13930	---	---
30	7749	9011	10254	11334	---	---	---
31	5157	5917	6594	8011	9803	---	---
32	4775	5178	5613	6409	7489	8749	9504
33	3999	4335	4697	5373	6297	7364	7881
34	3982	4497	5086	5714	6894	8140	---
35	4586	5203	5862	7179	---	---	---
36	4472	5163	5798	7064	---	---	---
37	6455	7381	8577	---	---	---	---
38	4682	5736	---	---	---	---	---
39	4569	5373	6613	---	---	---	---
40	5504	6689	7918	---	---	---	---
41	3202	3977	4721	---	---	---	---
42	4712	5071	5964	7077	---	---	---
43	5504	6689	7918	---	---	---	---
44	3202	3977	4721	---	---	---	---
45	4712	5071	5964	7077	---	---	---
46	5530	6336	7325	---	---	---	---
47	4864	5432	6032	6665	---	---	---
48	5464	6599	7846	---	---	---	---
49	5198	5859	6665	8442	---	---	---
50	5845	6643	7493	9480	---	---	---
51	3717	3998	4340	5015	5917	---	---
52	3651	3933	4276	4900	5802	6786	---
53	3775	---	---	---	---	---	---
54	5616	---	---	---	---	---	---
55	5616	---	---	---	---	---	---

TABLE B-8: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 40°F , ELEVATION 6000 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	6652	7197	7766	9131	10964	13173	15186
3	5354	5838	6476	7288	9549	9876	---
4	3768	4215	4666	5400	6479	7636	9630
5	5302	5729	6174	7240	8665	10376	11928
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4053	4671	---	---
9	4553	5190	5772	6813	8304	9952	11187
10	2799	3128	3656	4424	5486	6037	---
11	3811	4305	4832	5682	6290	---	---
12	4564	5078	5902	7100	8756	10210	---
13	5627	6157	6997	8202	9846	10906	12405
14	4718	5175	5904	6956	8401	9338	10671
15	0	0	0	---	---	---	---
16	4553	5190	5772	6813	8304	9952	11187
17	5627	6157	6997	8202	9846	10906	12405
18	10014	10014	12293	12293	14074	14074	---
19	6158	6763	7616	8997	10501	12129	---
20	4687	5083	5496	6404	7684	9124	10817
21	7132	7748	8346	9706	11634	13801	16285
22	7182	7650	8383	9152	10801	12602	---
23	6614	7023	7661	8330	9659	11096	12698
24	5968	6863	7821	8841	---	---	---
25	6885	7634	8423	9376	---	---	---
26	8030	8898	10165	11906	13930	---	---
27	9155	10665	12295	13896	---	---	---
28	6885	7634	8423	9376	---	---	---
29	8030	8898	10165	11906	13930	---	---
30	7749	9011	10254	11334	---	---	---
31	5157	5917	6594	8011	9803	---	---
32	4775	5178	5613	6409	7489	8749	9504
33	3999	4335	4697	5373	6297	7364	7881
34	3982	4497	5086	5714	6894	8140	---
35	4586	5203	5862	7179	---	---	---
36	4472	5163	5798	7064	---	---	---
37	6455	7381	8577	---	---	---	---
38	4682	5736	---	---	---	---	---
39	4569	5373	6613	---	---	---	---
40	5504	6689	7918	---	---	---	---
41	3202	3977	4724	---	---	---	---
42	4712	5071	5964	7077	---	---	---
43	5504	6689	7918	---	---	---	---
44	3202	3977	4724	---	---	---	---
45	4712	5071	5964	7077	---	---	---
I 46	5530	I 6336	7325	---	---	---	---
47	4864	5432	6032	6665	---	---	---
48	5464	6599	7846	---	---	---	---
49	5198	5859	6665	8442	---	---	---
50	5845	6643	7493	9480	---	---	---
51	3717	3998	4340	5015	5917	---	---
52	3651	3933	4276	4900	5802	6786	---
53	3775	---	---	---	---	---	---
54	5616	---	---	---	---	---	---
55	5616	---	---	---	---	---	---

TABLE B-8: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 40°F , ELEVATION 6000 FT MSL

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
1	4358	4732	5223	5842	7545	7788	---
2	6652	7197	7766	9131	10964	13173	15186
3	5354	5838	6476	7288	9549	9876	---
4	3768	4215	4666	5400	6479	7636	9630
5	5302	5729	6174	7240	8665	10376	11928
6	4193	4671	5438	6551	8098	9433	---
7	3963	4429	5176	6263	7767	8547	---
8	2721	3109	3523	4053	4671	---	---
9	4553	5190	5772	6813	8304	9952	11187
10	2799	3128	3656	4424	5486	6037	---
11	3811	4305	4832	5682	6290	---	---
12	4564	5078	5902	7100	8756	10210	---
13	5627	6157	6997	8202	9846	10906	12405
14	4718	5175	5904	6956	8401	9338	10671
15	0	0	0	---	---	---	---
16	4553	5190	5772	6813	8304	9952	11187
17	5627	6157	6997	8202	9846	10906	12405
18	10014	10014	12293	12293	14074	14074	---
19	6158	6763	7616	8997	10501	12129	---
20	4687	5083	5496	6404	7684	9124	10817
21	7132	7748	8346	9706	11634	13801	16285
22	7182	7650	8383	9152	10801	12602	---
23	6614	7023	7661	8330	9659	11096	12698
24	5968	6863	7821	8841	---	---	---
25	6885	7634	8423	9376	---	---	---
26	8030	8898	10165	11906	13930	---	---
27	9155	10665	12295	13896	---	---	---
28	6885	7634	8423	9376	---	---	---
29	8030	8898	10165	11906	13930	---	---
30	7749	9011	10254	11334	---	---	---
31	5157	5917	6594	8011	9803	---	---
32	4775	5178	5613	6409	7489	8749	9504
33	3999	4335	4697	5373	6297	7364	7881
34	3982	4497	5086	5714	6894	8140	---
35	4586	5203	5862	7179	---	---	---
36	4472	5163	5798	7064	---	---	---
37	6455	7381	8577	---	---	---	---
38	4682	5736	---	---	---	---	---
39	4569	5373	6613	---	---	---	---
40	5504	6689	7918	---	---	---	---
41	3202	3977	4724	---	---	---	---
42	4712	5071	5964	7077	---	---	---
43	5504	6689	7918	---	---	---	---
44	3202	3977	4724	---	---	---	---
45	4712	5071	5964	7077	---	---	---
46	5530	6336	7925	---	---	---	---
47	4864	5432	6032	6665	---	---	---
48	5464	6599	7846	---	---	---	---
49	5198	5859	6665	8442	---	---	---
50	5845	6643	7493	9480	---	---	---
51	3717	3998	4340	5015	5917	---	---
52	3651	3933	4276	4900	5802	6786	---
53	3775	---	---	---	---	---	---
54	5616	---	---	---	---	---	---
55	5616	---	---	---	---	---	---

TABLE B-9:: RUNWAY REQUIREMENTS/OPERATIONAL BOUNDARIES OF THE PROFILE GENERATOR,  
TEMPERATURE 80°F , ELEVATION 6000 FT MSL (CONTINUED)

INM #	STAGE WEIGHT						
	1	2	3	4	5	6	7
56	4136	---	---	---	---	---	---
57	4807	---	---	---	---	---	---
58	5661	---	---	---	---	---	---
59	6766	---	---	---	---	---	---
60	4555	---	---	---	---	---	---
61	8001	---	---	---	---	---	---
62	6615	---	---	---	---	---	---
63	4414	5561	7505	---	---	---	---
64	2855	---	---	---	---	---	---
65	1982	---	---	---	---	---	---
66	6317	8054	9629	---	---	---	---
67	4318	---	---	---	---	---	---
68	4189	---	---	---	---	---	---
69	2028	---	---	---	---	---	---
70	5207	6876	8831	---	---	---	---
71	2487	3038	0	---	---	---	---
72	2933	3817	---	---	---	---	---
73	3408	---	---	---	---	---	---
74	1034	---	---	---	---	---	---
75	1208	---	---	---	---	---	---
76	2593	---	---	---	---	---	---
77	1148	---	---	---	---	---	---
78	18878	---	---	---	---	---	---
79	6840	10669	---	---	---	---	---
80	8500	11636	---	---	---	---	---
81	7374	11018	---	---	---	---	---
82	8381	0	---	---	---	---	---
83	6277	6983	7577	8842	10570	13065	15177
84	6848	7412	7973	9366	11237	13473	15537
85	6100	7090	7884	9609	---	---	---
86	9544	6401	7883	9795	---	---	---
87	4787	5190	5626	6444	7559	8853	9478
88	0	0	0	---	---	---	---
89	9178	6354	7489	---	---	---	---
90	9938	6764	8124	---	---	---	---
91	18717	---	---	---	---	---	---
92	15377	---	---	---	---	---	---
93	9501	6097	6970	8169	9569	---	---
94	5181	5896	6462	7193	---	---	---
95	4880	---	---	---	---	---	---
96	7277	---	---	---	---	---	---
97	6660	7926	9440	10953	---	---	---
98	6909	---	---	---	---	---	---
99	3855	---	---	---	---	---	---
100	4513	5004	5522	6146	---	---	---
101	5460	6050	6913	8098	9476	---	---
102	7503	8107	8737	10302	12006	14124	16729
103	7878	8519	9187	10851	12665	14926	17713
104	3000	---	---	---	---	---	---
105	3000	---	---	---	---	---	---
106	3000	---	---	---	---	---	---
107	3000	---	---	---	---	---	---

## APPENDIX C

### AIRPLANE RUNUP OPERATIONS

This Appendix discusses the adaptation of an existing **INM** equation for use in computing **runup** noise within **INM** Version 4.11. This equation, also used in the Time-Above-Threshold (**TA**) equation, can be used to approximate the maximum A-weighted sound level ( $L_{MAX}$ ) and the maximum tone-corrected perceived noise level ( $PNLT_{MAX}$ ) for a one-second time period as follows:

$$L_{MAX} = SEL - 10 \log_{10} [ ((500\pi) / (V)) (.001R_0)^k ] \text{ and} \quad (1)$$

$$PNLT_{MAX} = EPNL - 10 \log_{10} [ ((500\pi) / (V)) (.001R_0)^k ] + 10, \quad (2)$$

where

<b>SEL</b>	=	the Sound Exposure Level from the Noise-Power-Distance data base ( <b>dba</b> );
<b>EPNL</b>	=	the Effective Perceived Noise Level from the <del>Noise-Power</del> -Distance data base ( <b>db</b> );
<b>v</b>	=	the airplane velocity ( <b>ft/sec</b> );
<b>R<sub>0</sub></b>	=	the closest point of approach from airplane to receiver ( <b>ft</b> );
<b>k</b>	=	a constant exponent with a fixed value of <b>0.6</b> in the <b>INM</b> ; and for Equation (2),
<b>10</b>	=	a duration correction as discussed in Section 2.3, Equation (2).

The above equations assume: (1) an approximate shape of an airplane's sound level time history; and (2) symmetry in the time history trace around the  $L_{MAX}$  or  $PNLT_{MAX}$ , as appropriate. The  $L_{MAX}/PNLT_{MAX}$  values computed with these equations were verified using measured  $L_{MAX}/PNLT_{MAX}$  data in the literature.'

Given the computed  $L_{MAX}/PNLT_{MAX}$  and the user-defined duration and location for a **runup**, the **SEL/EPNL** for the **runup** is computed by multiplying the acoustic energy associated with the  $L_{MAX}/PNLT_{MAX}$  by the user-defined duration, and converting the total **runup** energy to a decibel value as follows:

$$SEL_{RUNUP} = 10 \log_{10} [ (DUR) 10^{(L_{MAX}/10)} ] \text{ and} \quad (3)$$

## APPENDIX C

### AIRPLANE RUNUP OPERATIONS

This Appendix discusses the adaptation of an existing **INM** equation for use in computing **runup** noise within **INM** Version 4.11. This equation, also used in the Time-Above-Threshold (**TA**) equation, can be used to approximate the maximum A-weighted sound level ( $L_{MAX}$ ) and the maximum tone-corrected perceived noise level ( $PNLT_{MAX}$ ) for a one-second time period as follows:

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$$PNLT_{MAX} = EPNL - 10 \log_{10} [ ((500m) / (V)) (.001R_0)^k ] + 10, \quad (2)$$

where

<b>SEL</b>	=	the Sound Exposure Level from the Noise-Power-Distance data base ( <b>dB</b> );
<b>EPNL</b>	=	the Effective Perceived Noise Level from the <del>Noise-Power</del> -Distance data base ( <b>dB</b> );
<b>v</b>	=	the airplane velocity ( <b>ft/sec</b> );
<b>R<sub>0</sub></b>	=	the closest point of approach from airplane to receiver ( <b>ft</b> );
<b>k</b>	=	a constant exponent with a fixed value of <b>0.6</b> in the <b>INM</b> ; and for Equation (2),
<b>10</b>	=	a duration correction as discussed in Section 2.3, Equation (2).

The above equations assume: (1) an approximate shape of an airplane's sound level time history; and (2) symmetry in the time history trace around the  $L_{MAX}$  or  $PNLT_{MAX}$ , as appropriate. The  $L_{MAX}/PNLT_{MAX}$  values computed with these equations were verified using measured  $L_{MAX}/PNLT_{MAX}$  data in the literature.'

Given the computed  $L_{MAX}/PNLT_{MAX}$  and the user-defined duration and location for a **runup**, the **SEL/EPNL** for the **runup** is computed by multiplying the acoustic energy associated with the  $L_{MAX}/PNLT_{MAX}$  by the user-defined duration, and converting the total **runup** energy to a decibel value as follows:

$$SEL_{RUNUP} = 10 \log_{10} [ (DUR) 10^{(L_{MAX}/10)} ] \text{ and} \quad (3)$$

**directivity** pattern discussed in Appendix A is a reasonable approximation of **runup directivity**.

## **C.2** References

- <sup>1</sup> Bishop, **D.E.**, Beckman, **J.M.**, ~~Bucka, M.P.~~, Revision of Civil Aircraft Noise Data for the **Integrated** Noise Model (INM), Report No. **6039**, Project No. **04453**, **Canoga** Park, CA: **BBN** Laboratories Incorporated, September **1986**.
- <sup>2</sup> **A320** Noise Definition Manual **NDM**, FRANCE: **Airbus Industrie**, 1990.
- <sup>3</sup> An Excerpt from the Model **B747** Flight Manual, **A-Weighted Noise Level Contours**, Seattle, WA: Boeing Commercial Airplane Company, **1986**.



**directivity** pattern discussed in Appendix A is a reasonable approximation of **runup directivity**.

## **C.2** References

- <sup>1</sup> Bishop, D.E., Beckman, J.M., ~~Bucka, M.P.~~, Revision of Civil Aircraft Noise Data for the Integrated Noise Model (INM), Report No. ~~6039~~, Project No. ~~04453~~, Canoga Park, CA: BBN Laboratories Incorporated, September ~~1986~~.
- <sup>2</sup> A320 Noise Definition Manual NDM, FRANCE: ~~Airbus Industrie~~, 1990.
- <sup>3</sup> An Excerpt from the Model ~~B747~~ Flight Manual, A-Weighted Noise Level Contours, Seattle, WA: Boeing Commercial Airplane Company, 1986..

**directivity** pattern discussed in Appendix A is a reasonable approximation of **runup directivity**.

## **C.2** References

- <sup>1</sup> Bishop, D.E., Beckman, J.M., ~~Bucka, M.P.~~, Revision of Civil Aircraft Noise Data for the Integrated Noise Model (INM), Report No. ~~6039~~, Project No. ~~04453~~, Canoga Park, CA: BBN Laboratories Incorporated, September ~~1986~~.
- <sup>2</sup> A320 Noise Definition Manual NDM, FRANCE: ~~Airbus Industrie~~, 1990.
- <sup>3</sup> An Excerpt from the Model ~~B747~~ Flight Manual, A-Weighted Noise Level Contours, Seattle, WA: Boeing Commercial Airplane Company, 1986..

BEGIN.

COMMENTS:

SETUP:

TITLE <ANNUAL AVERAGE EXPOSURE AT AN EXAMPLE OF A MEDIUM HUB AIRPORT>  
AIRPORT <EXAMPLE MHA>

ALTITUDE 0  
TEMPERATURE 59 F

RUNWAYS

RW 09L-27R	0	0	TO 9487	-497	HEADING=93
RW 27L-09R	4203	-1410	TO -6920	-1044	HEADING=272
RW 35-17	7355	1366	DT 100 TO 6407	6742	

Note: Standard conditions have been defined. To implement the takeoff profile generator ~~see~~ Section 2.1. In addition, the ~~elevation enhancement has not been selected.~~  
To implement elevation ~~see~~ Section 2.2.

AIRCRAFT:

TYPES

AC 747200  
AC DC1030  
AC DC870  
AC A300  
AC 757PW  
AC 727Q15  
AC DC930  
AC MD81  
AC 737300  
AC SABB30  
AC BECSBP  
AC S-76 CURVE=250C30 PARAM=HELI STAGE 1=HORFLT  
CATEGORY=PGA

Note: A runway touch-down point of 1054 ft has been defined for approach operations on Runway 35 (i.e., 100 ft for the ~~user-defined~~ DT plus 954 ft for the fixed touch-down point).

NOISE CURVES

NC 250C30 3 BY 8 3 BY 8

EPNL

THRUSTS	1	2	3
200	90.2	91.2	97.2
400	85.8	87.2	93.1
600	83.1	84.5	90.6
1000	79.4	80.7	87.4
2000	73.7	75.1	82.6
4000	67.6	68.2	77.2
6000	63.1	63.8	73.7
10000	56.8	57.4	68.7

SEL

THRUSTS	1	2	3
200	88.6	90.0	95.6
400	84.2	85.6	91.5
600	81.5	82.9	89.0
1000	77.8	79.1	85.8
2000	72.1	73.5	81.0
4000	66.0	66.6	75.6
6000	61.5	62.2	72.1
10000	55.2	55.8	67.1

APPROACH PARAMETERS

AP HELI WEIGHT=10000 ENGINE=2 STOP=1  
FINSF=160 TAXI=160  
LNDFFS=3

INT.NM.

PROFILES APPROACH

PF ALT3D SEGMENTS=7

DISTANCES	20.	10.	5.	3.	1.	-.164	STOP
ALTITUDES	6000	3236	1644	1007	370	0	0
SPEEDS	TERMSF	INTSF	APPSF	FINSF	LNDSP	REVSP	TAXI
THRUSTS	INTFIS	APPFAS	LNDFFS	LNDFLS	REV	IDLE	

PF COPTER SEGMENTS=7

DISTANCES	3.9	3.1	2.4	1.6	0.8	0	0
ALTITUDES	2500	2000	1500	1000	500	0	0
SPEEDS	FINSF	FINSF	FINSF	FINSF	FINSF	FINSF	TAXI
THRUSTS	LNDFFS	LNDFFS	LNDFFS	LNDFFS	LNDFFS	LNDFFS	

ECHO.

FT.

PROFILES TAKEOFF

PF HORFLT SEGMENTS=8 WEIGHT=10000 ENGINES=2

DISTANCES	0	1376	4126	6876	6877	9626	10000	15000
ALTITUDES	0	0	500	1000	1000	1500	1500	1500
SPEEDS	32	160	160	160	160	160	160	160
THRUSTS	2	2	2	2	1	1	1	

INT.NM.

COMMENTS :

TAKEOFFS BY FREQUENCY:

TRACK TR1 RWY 09L STRAIGHT 4.1 LEFT 5 H 1.6 STRAIGHT 50  
OPER 747200 RUNUP 1 D=10 STAGE 1 D=1.1 STAGE 2 D=1.1 STAGE 3 D=1.1  
OPER DC1030 STAGE 1 D=1.5 STAGE 2 D=2.5 STAGE 4 D=2  
OPER 757PW STAGE 2 D=1.5  
OPER 727Q15 STAGE 1 D=3 N=.5 STAGE 2 D=2.6 N=.6  
STAGE 3 D=1.2 N=.1  
OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5  
STAGE 3 D=1.5  
OPER MD81 STAGE 2 D=1.0  
OPER 737300 STAGE 1 D=1.5 N=.5

Note: A **runup** operation has been defined for the B747-200 airplane. The **runup** takes place at the start of Runway 09L and lasts for 10 seconds, (i.e., in terms of average yearly duration).

TRACK TR2 RWY 27R STRAIGHT 4.1 LEFT 88 D 1.6 STRAIGHT 50  
OPER DC1030 STAGE 1 D=1.5 STAGE 2 D=3 STAGE 3 D=1  
STAGE 4 D=1 STAGE 5 D=.5 STAGE 6 D=.5  
OPER DC870 STAGE 1 D=2 N=.5 STAGE 2 D=3.5 N=1  
STAGE 3 D=1 STAGE 4 D=2.5 STAGE 5 D=1  
STAGE 6 D=.5  
OPER A300 STAGE 2 D=2 STAGE 3 D=1  
OPER 727Q15 STAGE 1 D=6 N=1 STAGE 2 D=4.4 N=1.4 STAGE 3 D=1.8  
N=.4

TRACK TR3 RWY 09R STRAIGHT 1.3 LEFT 15 D 1.0 STRAIGHT 1.4  
RIGHT 57 D 1.8 STRAIGHT .5 RIGHT 50 D 1.6  
STRAIGHT 50  
OPER DC870 STAGE 1 D=2 N=.5 STAGE 2 D=3.5 N=1 STAGE 3 D=1  
STAGE 4 D=1.5 STAGE 5 D=.5  
OPER 757PW STAGE 3 D=2.5  
OPER 727Q15 STAGE 1 D=21 N=2.5 STAGE 2 D=16.5 N=4  
STAGE 3 D=8 N=.5  
OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5 STAGE 3 D=1.5  
OPER MD81 STAGE 1 D=3 N=.5  
OPER 737300 STAGE 2 D=.5

TRACK TR4 RWY 27R STRAIGHT 4.1 LEFT 230 H 2.2 STRAIGHT 50  
OPER SABRE0 STAGE 1 D=3 N=.1

TRACK TR5 RWY 35 STRAIGHT 50  
OPER SABRE0 STAGE 1 D=30.5 N=2.5  
OPER BEC58P STAGE 1 D=13 N=1

TRACK TR6 RWY 17 STRAIGHT 50  
OPER SABRE0 STAGE 1 D=12.5 N=.5  
OPER BEC58P STAGE 1 D=30 N=3

TRACK TR7 RWY 17 STRAIGHT 1.5 RIGHT 265 H .25 STRAIGHT 3  
LEFT 245 H 1.0 STRAIGHT 50  
OPER S-76 STAGE 1 D=5

LANDINGS BY PERCENTAGE:

OPER 747200 PROF=STD3D D=3 N=0  
OPER DC1030 PROF=STD3D D=22 N=2  
OPER DC870 PROF=ALT3D D=22 N=2  
OPER A300 PROF=STD3D D=2 N=1  
OPER 757PW PROF=STD3D D=6 N=1  
OPER 727Q15 PROF=ALT3D D=70 N=10  
OPER DC930 PROF=ALT3D D=70 N=4  
OPER MD81 PROF=STD3D D=4 N=.5  
OPER 737300 PROF=STD3D D=1.5 N=.5  
OPER SABRE0 PROF=STD3D D=25 N=2  
OPER BEC58P PROF=STD3D D=42 N=5  
OPER S-76 PROF=COPTR D=5

TRACK TR8 RWY 27R STRAIGHT 50 RIGHT 82 D 1.5 STRAIGHT 4.2  
PERCENT COM=72 GA=0

TRACK TR9 RWY 09R HEADING 260 STRAIGHT 50 RIGHT 272 H 1.5  
STRAIGHT 7 PERCENT COM=28 GA=0

TRACK TR10 RWY 35 STRAIGHT 50 PERCENT COM=0 GA=30

TRACK TR11 RWY 17 STRAIGHT 50 PERCENT COM=0 GA=70

TOUCHNGOS BY FREQUENCY:

TRACK TR14 RWY 17 STRAIGHT 3 LEFT 180 D 2.0 STRAIGHT 6  
LEFT 180 D 2.0 STRAIGHT 3  
OPER BEC58P STAGE 1 PROF STD5D D=23

INT.NM.

COMMENTS :

TAKEOFFS BY FREQUENCY:

TRACK TR1 RWY 09L STRAIGHT 4.1 LEFT 5 H 1.6 STRAIGHT 50  
OPER 747200 RUNUP 1 D=10 STAGE 1 D=1.1 STAGE 2 D=1.1 STAGE 3 D=1.1  
OPER DC1030 STAGE 1 D=1.5 STAGE 2 D=2.5 STAGE 4 D=2  
OPER 757PW STAGE 2 D=1.5  
OPER 727Q15 STAGE 1 D=3 N=.5 STAGE 2 D=2.6 N=.6  
STAGE 3 D=1.2 N=.1  
OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5  
STAGE 3 D=1.5  
OPER MD81 STAGE 2 D=1.0  
OPER 737300 STAGE 1 D=1.5 N=.5

Note: A **runup** operation has been defined for the B747-200 airplane. The **runup** takes place at the start of Runway 09L and lasts for 10 seconds, (i.e., in terms of average yearly duration).

TRACK TR2 RWY 27R STRAIGHT 4.1 LEFT 88 D 1.6 STRAIGHT 50  
OPER DC1030 STAGE 1 D=1.5 STAGE 2 D=3 STAGE 3 D=1  
STAGE 4 D=1 STAGE 5 D=.5 STAGE 6 D=.5  
OPER DC870 STAGE 1 D=2 N=.5 STAGE 2 D=3.5 N=1  
STAGE 3 D=1 STAGE 4 D=2.5 STAGE 5 D=1  
STAGE 6 D=.5  
OPER A300 STAGE 2 D=2 STAGE 3 D=1  
OPER 727Q15 STAGE 1 D=6 N=1 STAGE 2 D=4.4 N=1.4 STAGE 3 D=1.8  
N=.4

TRACK TR3 RWY 09R STRAIGHT 1.3 LEFT 15 D 1.0 STRAIGHT 1.4  
RIGHT 57 D 1.8 STRAIGHT .5 RIGHT 50 D 1.6  
STRAIGHT 50  
OPER DC870 STAGE 1 D=2 N=.5 STAGE 2 D=3.5 N=1 STAGE 3 D=1  
STAGE 4 D=1.5 STAGE 5 D=.5  
OPER 757PW STAGE 3 D=2.5  
OPER 727Q15 STAGE 1 D=21 N=2.5 STAGE 2 D=16.5 N=4  
STAGE 3 D=8 N=.5  
OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5 STAGE 3 D=1.5  
OPER MD81 STAGE 1 D=3 N=.5  
OPER 737300 STAGE 2 D=.5

TRACK TR4 RWY 27R STRAIGHT 4.1 LEFT 230 H 2.2 STRAIGHT 50  
OPER SABRE0 STAGE 1 D=3 N=.1

TRACK TR5 RWY 35 STRAIGHT 50  
OPER SABRE0 STAGE 1 D=30.5 N=2.5  
OPER BEC58P STAGE 1 D=13 N=1

TRACK TR6 RWY 17 STRAIGHT 50  
OPER SABRE0 STAGE 1 D=12.5 N=.5  
OPER BEC58P STAGE 1 D=30 N=3

TRACK TR7 RWY 17 STRAIGHT 1.5 RIGHT 265 H .25 STRAIGHT 3  
LEFT 245 H 1.0 STRAIGHT 50  
OPER S-76 STAGE 1 D=5

LANDINGS BY PERCENTAGE:

OPER 747200 PROF=STDD D=3 N=0  
OPER DC1030 PROF=STDD D=22 N=2  
OPER DC870 PROF=STDD D=22 N=2  
OPER A300 PROF=STDD D=2 N=1  
OPER 757PW PROF=STDD D=6 N=1  
OPER 727Q15 PROF=STDD D=70 N=10  
OPER DC930 PROF=STDD D=70 N=4  
OPER MD81 PROF=STDD D=4 N=.5  
OPER 737300 PROF=STDD D=1.5 N=.5  
OPER SABRE0 PROF=STDD D=25 N=2  
OPER BEC58P PROF=STDD D=42 N=5  
OPER S-76 PROF=COPTR D=5

TRACK TR8 RWY 27R STRAIGHT 50 RIGHT 82 D 1.5 STRAIGHT 4.2  
PERCENT COM=72 GA=0

TRACK TR9 RWY 09R HEADING 260 STRAIGHT 50 RIGHT 272 H 1.5  
STRAIGHT 7 PERCENT COM=28 GA=0

TRACK TR10 RWY 35 STRAIGHT 50 PERCENT COM=0 GA=30

TRACK TR11 RWY 17 STRAIGHT 50 PERCENT COM=0 GA=70

TOUCHINGS BY FREQUENCY:

TRACK TR14 RWY 17 STRAIGHT 3 LEFT 180 D 2.0 STRAIGHT 6  
LEFT 180 D 2.0 STRAIGHT 3  
OPER BEC58P STAGE 1 PROF STD50 D=23

INT.NM.

COMMENTS :

TAKEOFFS BY FREQUENCY:

TRACK TR1 RWY 09L STRAIGHT 4.1 LEFT 5 H 1.6 STRAIGHT 50  
OPER 747200 RUNUP 1 D=10 STAGE 1 D=1.1 STAGE 2 D=1.1 STAGE 3 D=1.1  
OPER DC1030 STAGE 1 D=1.5 STAGE 2 D=2.5 STAGE 4 D=2  
OPER 757PW STAGE 2 D=1.5  
OPER 727Q15 STAGE 1 D=3 N=.5 STAGE 2 D=2.6 N=.6  
STAGE 3 D=1.2 N=.1  
OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5  
STAGE 3 D=1.5  
OPER MD81 STAGE 2 D=1.0  
OPER 737300 STAGE 1 D=1.5 N=.5

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OPER DC930 STAGE 1 D=26.5 N=.5 STAGE 2 D=8 N=.5 STAGE 3 D=1.5  
OPER MD81 STAGE 1 D=3 N=.5  
OPER 737300 STAGE 2 D=.5

TRACK TR4 RWY 27R STRAIGHT 4.1 LEFT 230 H 2.2 STRAIGHT 50  
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LEFT 245 H 1.0 STRAIGHT 50  
OPER S-76 STAGE 1 D=5

LANDINGS BY PERCENTAGE:

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OPER A300 PROF=STDD D=2 N=1  
OPER 757PW PROF=STDD D=6 N=1  
OPER 727Q15 PROF=STDD D=70 N=10  
OPER DC930 PROF=STDD D=70 N=4  
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INT.NM.

COMMENTS :

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OPER 727Q15 STAGE 1 D=3 N=.5 STAGE 2 D=2.6 N=.6  
STAGE 3 D=1.2 N=.1  
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STAGE 3 D=1.5  
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## 1.0 INTRODUCTION

This User Guide is a combined tutorial-manual that comes to you as part of **WINM4.11**.

## 2.0 OPERATIONAL REQUIREMENTS

### **Software/Hardware Requirements**

**WINM** has the same **software** and hardware requirements as Microsoft Windows 3.x.

## 3.0 INSTALLATION

Before you start, make sure that you have **all** the material supplied with **WINM 4.11** and check that your equipment matches the list in Chapter 2.

### **Installation Procedure**

**WINM** comes with four files under the directory **WINM4.11**. These files will be installed as part of the primary **INM** installation. They are:

<b>WINMEXE</b>	- The window plot program for <b>INM</b>
<b>INMINPUT.TST</b>	- Test case version of input data
<b>CONTOURS.TST</b>	- Test case version of contour data
<b>INMCOLOR.DAT</b>	- Color control file

### **Windows Installation of WINM**

- Start up Windows by typing WIN.
- Open Windows' *Program Manager*.
- Open the Windows ***File*** menu. Select ***New***.
- The New *Program Object* dialog box will appear.
- Select ***Program Group*** and click on ***OK***.
- The ***Program Group Properties*** dialog box will appear.
- Type **WINM** in the *Description* field. Click on ***OK***.
- Open the Windows ***File*** menu. Select ***New***.
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- Select ***Program Item*** and click on ***OK***.



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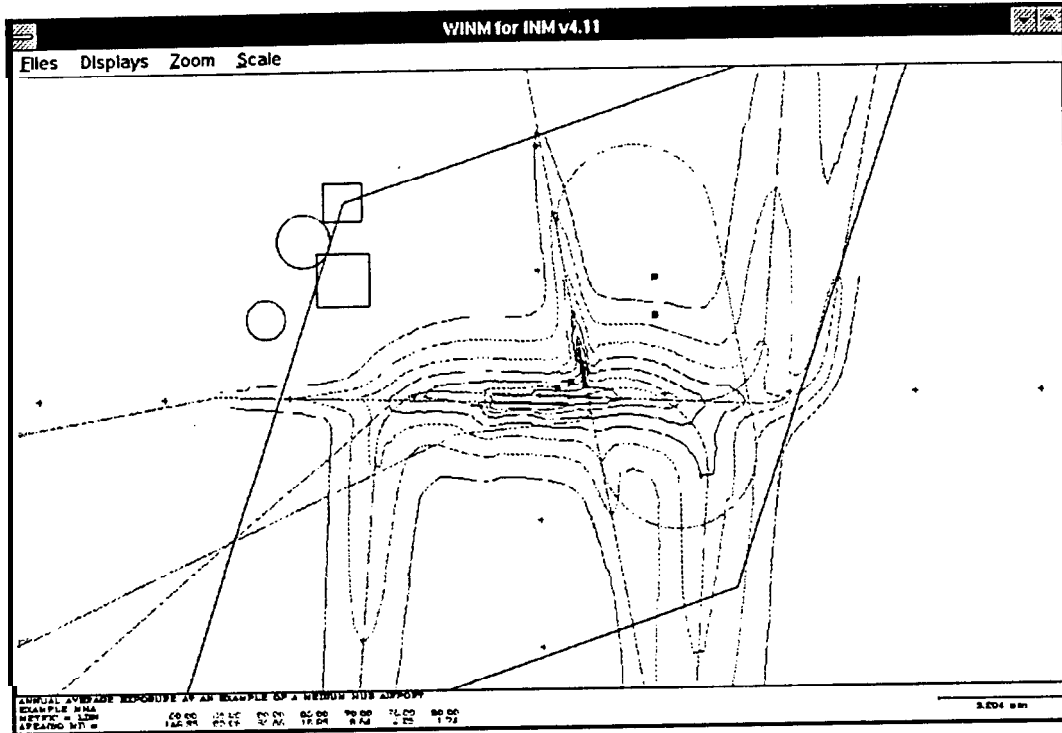
## 4.0 TUTORIAL

### About the Tutorial

The tutorial has been structured so that the exercises will give you progressive familiarity with the operations that you will carry out within **WINM 4.11**.

### 4.1 Loading INM Files

The starting point for this exercise is the default screen you see as soon as you start **WINM 4.11** from the Windows *Program Manager*.



By default, **WINM** uses two default **INM** input files. To load a different set of input files,

- Place the mouse pointer arrow on **Files** in the menu bar; and
- Click once on the left mouse button.
- In the menu, click the mouse pointer on **Load**.

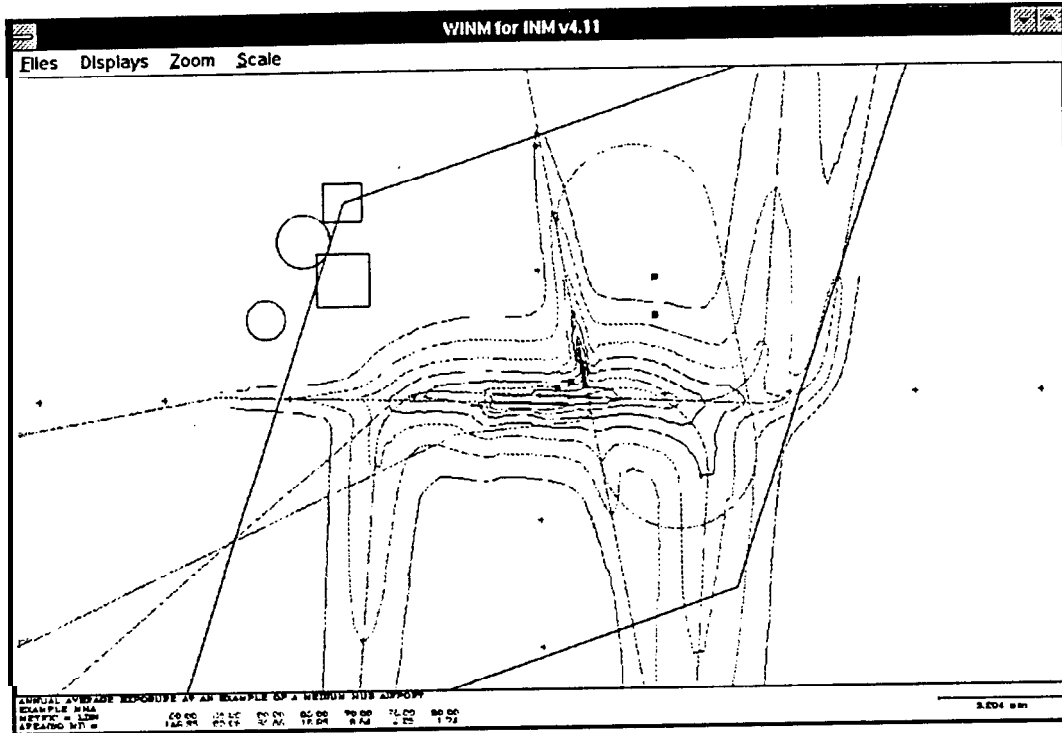
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## About the Displays Dialog Box

This menu option allows the user to select which data display information is to be shown. Select any option one at a time and click on **Apply** to see its effect immediately. Experiment with as many combinations as you like. Text labels may be independently selected for each displayed item type by clicking on the *Label* box next to each item.

### 4.2.1 Runways

This radio button turns on/off the display of the runways.

### 4.2.2 Flight Tracks

This radio button turns on/off the display of the flight tracks.

### 4.2.3 Noise Contours

This radio button turns on/off the display of the noise contours.

### 4.2.4 Fill Contours

This radio button turns on/off the option to fill the contours.

### 4.2.5 Noise Sensitive Area

Although every one of these options depends on the **INM** input files selected, the *Noise Sensitive Area* is a special option. This menu option displays **user-defined** sensitive noise areas. These areas are defined after the END statement of the **INM** input data file (**FOR03.DAT**), and each can be either a polygon, square, circle, or point. The area can be defined in NM or FEET and a descriptive text label for label description of the area can be inserted **after** an asterisk (\*) at the end of the line. The user can **input/modify** these data before or after running the noise model (but not during running the **WINM** program). The following shows an example of the descriptive text labels as seen in the default **INM** input filename **wininput.TSP**:

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## 4.3 Z o o m

### About the Zoom Menu

**WINM 4.11** offers you the capabilities to zoom in/out of various sections of the display for specialize viewing.

We will now become familiarized with the zooming capabilities within **WINM 4.11**.

- Place the mouse pointer arrow on ***Zoom*** in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down ***Zoom*** menu appear.

- In the menu, click the mouse pointer on ***Zoom In.***

A zoom box will appear in the center of the screen,

- Move the mouse to expand/shrink the zoom box.
- If you desire to move the zoom area, hold down the right button and drag the zoom box to a different area.
- Click the left button to accept zoom.

Note! At any time, click the right button to cancel the zoom box.

***Zoom Out*** works similar to ***Zoom In.***

- Place the mouse pointer arrow on ***Zoom*** in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down ***Zoom*** menu appear.

- In the menu, click the mouse pointer on ***Zoom Out.***

A zoom box will appear.

- Move the mouse to expand/shrink the zoom box.
- If you desire to move the zoom area, hold down the right button and drag the zoom box to a different area.

## 4.3 Z o o m

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***Zoom Out*** works similar to ***Zoom In.***

- Place the mouse pointer arrow on ***Zoom*** in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down ***Zoom*** menu appear.

- In the menu, click the mouse pointer on ***Zoom Out.***

A zoom box will appear.

- Move the mouse to expand/shrink the zoom box.
- If you desire to move the zoom area, hold down the right button and drag the zoom box to a different area.

You will see the drop-down *Scale* menu appear.

- In the menu, click the mouse pointer on any of the menu selections to see its effect to the scale shown at the bottom right-hand corner.

We have now covered the major capabilities of **WINM 4.11**.

Let's print the display to a printer.

- Place the mouse pointer arrow on ***F*iles** in the menu bar; and
- Click once on the left mouse button.

You will see the drop-down ***F*iles** menu appear.

- In the menu, click the mouse pointer on ***P*rint**. A submenu will appear.

## **4.5 Print**

### **About the Print Menu Option**

This menu option allows a hard copy output to a printer. The printout will go to the default printer which can be set via **Printers in Control Panel**.

- **Actual Scale**

This menu option allows the user to print the current screen for scaling. The scale unit will reflect 1 inch on the hardcopy printout.

- **Screen Zoom**

This menu option allows the user to print the current screen at the current zoom factor. The **left** and right edges of the hardcopy printout will be set to match the left and right edges of the screen display. If the printer's page orientation is set to 'Landscape' in the Windows **Print Manager**, then the top and bottom edges of the hardcopy printout will be set to match the top and bottom edges of the screen display as well.

To print what is displayed, select **Screen Zoom**

You can now exit the program.



You will see the drop-down *Scale* menu appear.

- In the menu, click the mouse pointer on any of the menu selections to see its effect to the scale shown at the bottom right-hand corner.

We have now covered the major capabilities of **WINM 4.11**.

Let's print the display to a printer.

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To print what is displayed, select ***S*creen *Z*oom**

You can now exit the program.

You will see the drop-down *Scale* menu appear.

- In the menu, click the mouse pointer on any of the menu selections to see its effect to the scale shown at the bottom right-hand corner.

We have now covered the major capabilities of **WINM 4.11**.

Let's print the display to a printer.

- Place the mouse pointer arrow on ***Files*** in the menu bar; and
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You will see the drop-down ***Files*** menu appear.

- In the menu, click the mouse pointer on ***Print***. A submenu will appear.

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To print what is displayed, select ***Screen Zoom***.

You can now exit the program.

## **6.0 Program Limitation.**

- Maximum **2000** points per noise contour.
- Runways information input is in FEET (from **INM** input file).
- Tracks information input is in NM (from **INM** input file).
- Shade pattern on hard copy may not be the same as on the screen due to the incompatibility number of colors support by the display and the printer.

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~~DOT-VNTSC-FAA-93-19~~

Office of Environment  
and Energy  
Washington, DC ~~20591~~

**INM**

# Integrated Noise Model Version 4.111

## User's Guide - Supplement

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John **R. D'Aprile**

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Transportation Systems Center  
Acoustics Facility  
Cambridge, MA ~~02142-1093~~

Final Report  
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Supplement to  
Report No. ~~DOT/FAA/EE/92/02~~

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Federal Aviation Administration

